

# **Standard** ECMA-328-1

9<sup>th</sup> Edition / December 2018

## **Determination of Chemical Emission Rates from Electronic Equipment – Part 1 (using-consumables)**

# Standard



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## Introduction

Globally, governmental agencies, academic institutions, environmental organizations and manufacturers have started to develop methods to determine chemical emissions from electronic equipment. These attempts however, initially resulted in a range of tests from which the results were not necessarily comparable, either qualitatively or quantitatively.

Following the publications of the 1st edition of ECMA-328 in 2001 and the “Test method for the determination of emissions from Hard Copy Devices” (RAL-UZ 122), experts from the BAM and Ecma have collaborated to harmonise methods to determine the chemical emission rates from ICT & CE equipment in the 2nd edition.

In addition to stricter test procedures, the 2nd edition used generalised emission formulae, and their derivations developed in Annex C, to calculate emission rates from concentrations of analytes that are measured in Emission Test Chambers.

The 3rd edition was fully aligned with the 1st edition of ISO/IEC 28360:2007 adopted under ISO/IEC JTC 1 fast-track procedure and published in September 2007.

In addition, the 4th edition fixed a number of errata on ISO/IEC 28360:2007 that JTC 1/SC 28 identified.

Following the publications of the 4th edition of ECMA-328 and the “Test method for the determination of emissions from Hard Copy Devices” (RAL-UZ 122), experts from the BAM, WKI, JBMIA and Ecma have collaborated to harmonise methods to determine the Fine Particle (FP) and Ultrafine Particle (UFP) emissions from hard copy devices in the 5th edition.

The 6th edition was aligned with the 2nd edition of ISO/IEC 28360:2012, and it added a new ozone calculation method. “Test method for the determination of emission from Hard Copy Devices” (RAL-UZ 122) has been replaced by “Test method for the determination of emission from Hard Copy Devices” (RAL-UZ 171) published in January 2013. Therefore, “RAL-UZ 122 option” is replaced with “RAL-UZ 171 option” in the 6th edition.

The 7th edition of ECMA-328 is fully aligned with ISO/IEC 28360:2015.

The 8th edition was divided into a part for electronic equipment using consumables and a part for electronic equipment not using consumables as follows:

- Determination of Chemical Emission Rates from Electronic Equipment – Part 1 (using-consumables)
- Determination of Chemical Emission Rates from Electronic Equipment – Part 2 (not using-consumables)

The purpose of the split was to make the description of test procedures simpler (they included considerable differences between the two equipment categories) and to facilitate users’ understanding.

The 8th edition is fully aligned with “Test method for the determination of emission from Hard Copy Devices” (RAL-UZ 205).

This 9th edition is fully aligned with ISO/IEC 28360-1:2018.

This part of the Standard is Part 1.

This Ecma Standard was developed by Technical Committee 38 and was adopted by the General Assembly of December 2018.

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## Part 1

# Determination of Chemical Emission Rates from Electronic Equipment (using-consumables)

## 1 Scope

This document (all parts) specifies methods to determine chemical emission rates of [analyte](#) from [ICT & CE equipment](#) during intended operation in an Emission Test Chamber ([ETC](#)).

This document (all parts) includes specific methods for equipment using consumables, such as printers, and equipment not using consumables, such as monitors and PC's.

Part 1 specifies the methods to determine chemical emission rates of [analyte](#) from electronic equipment using consumables.

The methods comprise preparation, sampling (or monitoring) in a controlled ETC, storage and analysis, calculation and reporting of emission rates.

Emission rates from EUT may also be determined according to additional requirements identified by "RAL-UZ 205 Option".

Annex A specifies monochrome and colour print patterns for use in the operating phase of EUT using consumables.

The operational readiness of AMS is confirmed according to [Annex B](#).

Calculations use the generalised model and approximations thereof as developed in [Annex C](#).

The emission rates determined with this method may be used to compare equipment in the same class.

Predictions of "real indoor" *concentrations* from the determined *emission rates* are outside the scope of this document.

## 2 Conformance

Determinations of emission rates and total number of emitted particles conform to this document (Part 1) when:

1. Executed using a Quality Assurance Project Plan, Quality Assurance and Quality Control as specified in ISO 16000-9;
2. Tested in a controlled ETC as specified in [Clause 7](#);
3. Sampled/monitored and calculated as specified in [Clause 8](#) and [Annex B](#);
4. Reported as specified in [Clause 9](#).

For EUT using consumables, determinations according to additional requirements identified by "RAL-UZ 205 Option" herein conform to the RAL-UZ 205 Option.

### 3 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 554:1976, *Standard atmospheres for conditioning and/or testing – Specifications*

ISO 16000-3:2011, *Indoor air – Part 3: Determination of formaldehyde and other carbonyl compounds – Active sampling method*

ISO 16000-6:2011, *Indoor air – Part 6: Determination of volatile organic compounds in indoor and chamber air by active sampling on TENAX TA sorbent, thermal desorption and gas chromatography using MS/FID*

ISO 16000-9:2006, *Indoor air – Part 9: Determination of the emission of volatile organic compounds from building products and furnishing – Emission test chamber method*

ISO 16017-1:2000, *Indoor ambient and workplace air - Sampling and analysis of volatile organic compounds by sorbent tube / thermal desorption / capillary gas chromatography – Part 1: Pumped sampling*

CIE 15:2004, *Commission Internationale de l'Eclairage – Colorimetry, 3<sup>rd</sup> edition*

### 4 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

#### 4.1

##### **averaged concentration time series**

simple moving average of total particle number concentration ( $C_p$ ) over  $31 \pm 3$  seconds

#### 4.2

##### **averaged ozone concentration time series**

simple moving average of ozone concentration ( $CO_3$ ) over  $80 \pm 5$  seconds

#### 4.3

##### **aerosol**

[suspension](#) of fine [solid](#) particles and/or [liquid](#) droplets in a [gas](#)

#### 4.4

##### **aerosol measuring system**

##### **AMS**

device category for measuring the total particle number concentration of an aerosol within a size range at a certain frequency

NOTE CPC (4.8) and fast AMS (4.12) belong to AMS.

#### 4.5

##### **air exchange rate**

##### **n**

ratio (n) of the volume of clean air brought into the ETC per hour [ $m^3/h$ ] to the unloaded ETC volume [ $m^3$ ]

#### 4.6

##### **air velocity**

air speed [ $m/s$ ] measured in the unloaded ETC



#### **4.7**

##### **analyte**

volatile organic compounds (VOC), carbonyl compounds, ozone, particulate matter, fine particles (FP) and ultrafine particles (UFP)

#### **4.8**

##### **condensation particle counter**

##### **CPC**

instrument that measures the particle number concentration of an aerosol.

NOTE For the purpose of this document a CPC is used as a standalone instrument which measures the total particle number concentration within a device dependent size range

#### **4.9**

##### **consumables**

toner, ink, paper and ribbon

#### **4.10**

##### **emission test chamber**

##### **ETC**

enclosure with controlled operational parameters for testing analyte mass emitted from EUT

#### **4.11**

##### **equipment under test**

##### **EUT**

electronic equipment from which chemical emission rates are determined

#### **4.12**

##### **fast AMS**

instrument with rapid time resolution and particle size classification

#### **4.13**

##### **fine particles**

##### **FP**

particles with particle size / diameter range between 0.1  $\mu\text{m}$  and 2.5  $\mu\text{m}$

#### **4.14**

##### **hard copy devices**

class of EUT using consumables that includes printers, (Photo)copiers and Multi Functional Devices (MFD)

#### **4.15**

##### **loading factor**

ratio of the EUT volume to the volume of the unloaded ETC

#### **4.16**

##### **maximum usage time before testing**

##### **MUT**

ratio between the total number of prints carried out by the EUT and the printing speed of the EUT

NOTE Maximum usage time is the maximum permitted time of operation before testing in order to consider the EUT as newly manufactured equipment for testing purposes.

#### **4.17**

##### **operating phase**

phase in which the EUT is performing its intended functions

#### **4.18**

##### **particle**

solid or liquid matter with defined physical boundaries suspended in a gas

#### 4.19

##### **particle emission rate**

##### **PER**

averaged emission rate, i.e. total number of particles in a specified particle size range emitted during the operating phase

#### 4.20

##### **particle emission rate**

##### **PER(t)**

time dependent emission rate of particles in a specified particle size range after the start of the operating phase

#### 4.21

##### **particle loss coefficient**

##### **$\beta$**

coefficient describes the loss of particles in a specified particle size range in an ETC

#### 4.22

##### **particle size / particle diameter**

measurement category to describe the physical dimension of a particle

NOTE The term particle size is often used as a synonym for particle diameter. The particle diameter is used to assign a particle to a particle size class (e.g. UFP).

#### 4.23

##### **particulate matter**

##### **PM**

quantity of particles measured by gravimetric methods

#### 4.24

##### **post-operating phase**

phase following the operating phase

NOTE The post-operating can include energy saving modes.

#### 4.25

##### **pre-operating phase**

phase in which the EUT is connected to an electrical supply before the EUT is able to enter the operating phase

NOTE The pre-operating phase can include warming-up and energy saving modes.

#### 4.26

##### **standard particle emission rate**

PER<sub>10</sub> calculated number of particles emitted during a 10-minute operating phase in a specified particle size range

#### 4.27

##### **total number of emitted particles**

##### **TP**

calculated total number of particles emitted in a specified particle size range

#### 4.28

##### **total particle number concentration**

##### **C<sub>p</sub>**

particle number concentration in a specified particle size range

#### **4.29**

##### **total volatile organic compounds**

##### **TVOC**

the sum of the concentrations of identified VOC and the concentrations of the converted areas of unidentified peaks using the toluene response factor

NOTE This definition of “total volatile organic compounds” differs from the definition in ISO 16000-6:2011.

#### **4.30**

##### **ultrafine particles**

##### **UFP**

particles with particle diameter less or equal 0.1 µm

#### **4.31**

##### **unit specific emission rate**

##### **SER**

mass, in micrograms, of a specific analyte emitted per hour

#### **4.32**

##### **volatile organic compounds**

##### **VOC**

compounds that elute between n-hexane and n-hexadecane on a nonpolar GC-column

## **5 Symbols and abbreviated terms**

### **5.1 Abbreviated terms**

AMS	Aerosol Measuring System
CPC	Condensation Particle Counter
DNPH	2,4-Dinitrophenylhydrazine
ETC	Emission Test Chamber
EUT	Equipment Under Test
FID	Flame Ionisation Detector
FP	Fine Particles
GC/MS	Gas Chromatography/Mass Spectrometry
MFD	Multi Functional Device
PER	Averaged Particle Emission Rate
PER(t)	Time-dependent Particle Emission Rate
PER <sub>10</sub>	Standard Particle Emission Rate
PTFE	Polytetrafluoroethene (Polytetrafluoroethylene)
PVC	Polyvinylchloride
RH	Relative Humidity

SER	Unit Specific Emission Rate
TVOC	Total Volatile Organic Compounds
UFP	Ultrafine Particles
VOC	Volatile Organic Compounds

## 5.2 Symbols

$\alpha$	Factor in the exponential particle decay function [ $\text{cm}^{-3}$ ]
$\beta$	Particle loss coefficient [ $\text{h}^{-1}$ ]
$C_s$	Average mass concentration [ $\mu\text{g m}^{-3}$ ]
$C_{bg}$	Background mass concentration [ $\mu\text{g m}^{-3}$ ]
$C_0$	Initial mass concentration [ $\mu\text{g m}^{-3}$ ]
$C_{pre}$	Average mass concentration during pre-operating phase [ $\mu\text{g m}^{-3}$ ]
$C_{ope}$	Average mass concentration during operating phase and optionally during post-operating phase [ $\mu\text{g m}^{-3}$ ]
$C_p$	Total particle number concentration [ $\text{cm}^{-3}$ ]
$C_{pbg}$	Background particle number concentration [ $\text{cm}^{-3}$ ]
$\text{CO}_3$	Ozone concentration [ $\text{mg/m}^3$ ]
$d$	Equivalent Particle Diameter [ $\text{nm}$ ]
$m_{\text{after}}$	Sample filter mass [ $\mu\text{g}$ ] after sampling
$m_{\text{before}}$	Sample filter mass [ $\mu\text{g}$ ] before sampling
$m_{bg}$	Sampled mass for chamber background [ $\mu\text{g}$ ]
$m_{pm}$	Mass of particulate matter [ $\mu\text{g}$ ] deposited on the filter
$m_{\text{ref-after}}$	Reference filter mass [ $\mu\text{g}$ ] after sampling
$m_{\text{ref-before}}$	Reference filter mass [ $\mu\text{g}$ ] before sampling
$m_s$	Sampled mass [ $\mu\text{g}$ ]
$m_{pre}$	Sampled mass [ $\mu\text{g}$ ] during pre-operating phase
$m_{ope}$	Sampled mass [ $\mu\text{g}$ ] during operating and optionally post-operating phase
$n$	Air exchange rate [ $\text{h}^{-1}$ ]
$p$	Atmospheric pressure [ $\text{Pa}$ ]
$R$	Gas constant [ $\text{PaK}^{-1}$ ], (for ozone: $339.8 \text{ [PaK}^{-1})$ )
$SER_{bg}$	Background SER [ $\mu\text{g h}^{-1}$ ]

$SER_{ope}$	SER during operating and optionally post-operating phase [ $\mu\text{g h}^{-1}$ ]
$SER_{O_3}$	SER for ozone [ $\mu\text{g min}^{-1}$ ]
$SER_{pm}$	SER for particulate matter [ $\mu\text{g h}^{-1}$ ]
$SER_{pre}$	SER during pre-operating [ $\mu\text{g h}^{-1}$ ]
T	Ambient temperature [K]
TP	Total Number of Emitted Particles
$t_{ope}$	Operating phase duration [h]
$t_G$	Sampling time during operating and optionally post-operating phase [h]
$t_{start}$	Point in time marking the start of particle emission
$t_{stop}$	Point in time marking the end of particle emission
$t_{pre}$	Pre-operating phase duration [h]
$\Delta t$	Time-resolution of the UFP measurement [s]
V	ETC volume [ $\text{m}^3$ ]
$V_s$	Sampled air volume [ $\text{m}^3$ ]
$V_{bg}$	Sampled air volume [ $\text{m}^3$ ] for determination of $C_{bg}$
$V_{pre}$	Sampled air volume [ $\text{m}^3$ ] in pre-operating phase
$V_{ope}$	Sampled air volume [ $\text{m}^3$ ] in operating and optionally post-operating phase

## 6 Method overview

The flowchart in Figure 1 illustrates the method; clause numbers are indicated in brackets.

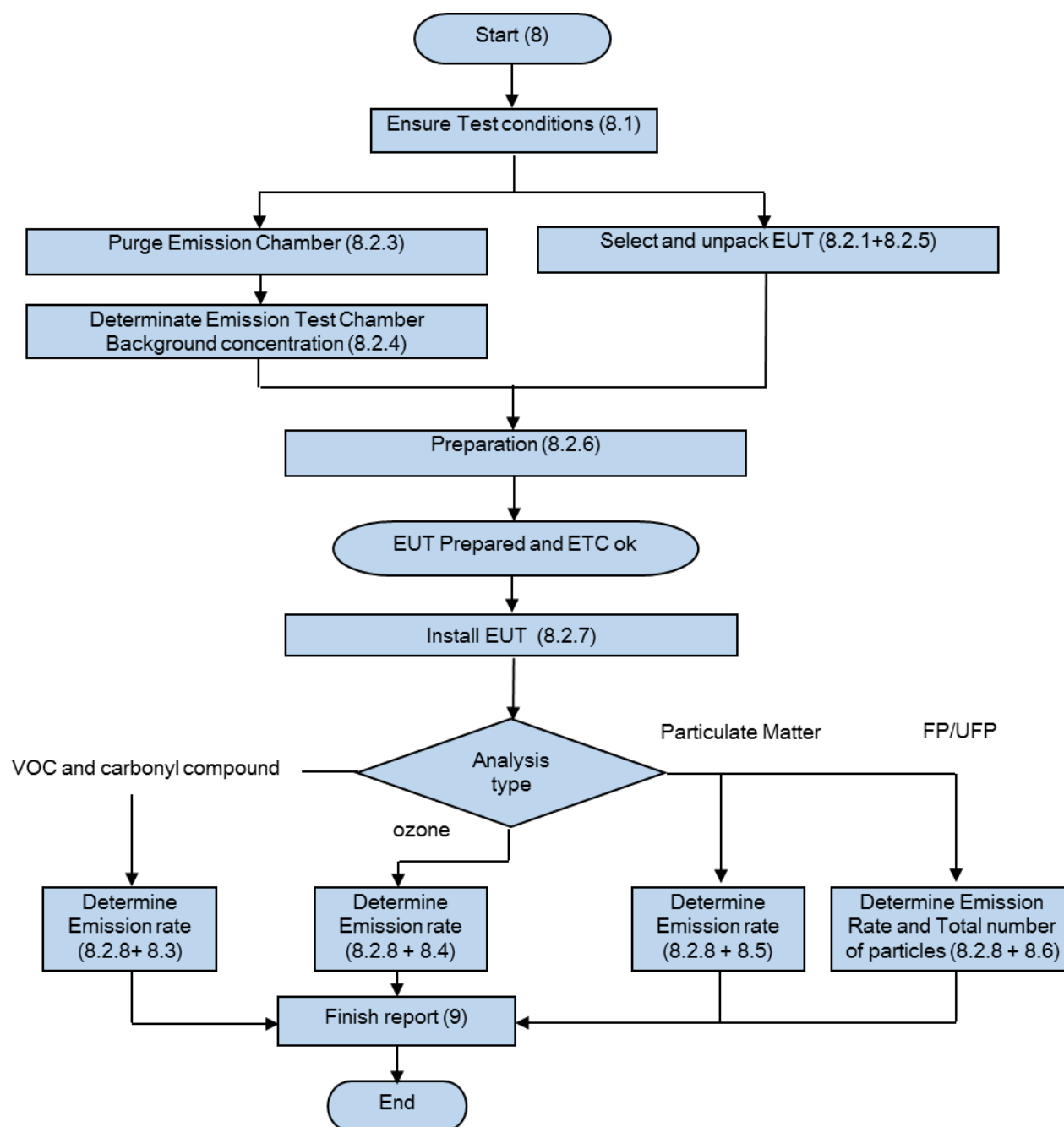


Figure 1 — Determination method overview

## **7 ETC requirements**

### **7.1 Construction materials**

ETC construction materials shall comply with ISO 16000-9.

### **7.2 Air tightness**

The ETC air tightness shall be as specified in ISO 16000-9.

### **7.3 Air mixing efficiency**

The air mixing efficiency in the ETC shall be as specified in ISO 16000-9.

## **8 Determination method**

### **8.1 Test conditions**

#### **8.1.1 General**

To meet the operational requirements specified herein, ETC parameters such as temperature, relative humidity and supply airflow shall be controlled and measured at regular intervals and recorded in accordance with ISO 16000-9 and shall be reported as specified in [Clause 9](#).

#### **8.1.2 Operating temperature and relative humidity (RH)**

Tests shall be executed at  $(23 \pm 2) ^\circ\text{C}$  and  $(50 \pm 5)\%$  RH according to ISO 554. For EUT used in alternative climatic conditions, higher operating temperature and humidity conditions may be used as specified in ISO 554.

Consult 8.2.8.3.2 for special requirements on RH for EUT using consumables.

#### **8.1.3 Air exchange rate (n)**

For unloaded ETCs with a volume larger than  $5 \text{ m}^3$ , n shall be in the range from 1,0 to 2,0. For unloaded ETC's with a volume of  $5 \text{ m}^3$  or smaller, n shall be in the range from 1,0 to 5,0.

#### **8.1.4 Air velocity**

The [air velocity](#) in the unloaded ETC shall be in the range from 0,1 to 0,3 m/s.

#### **8.1.5 Sampled air flow**

The sum of sampled airflow shall be less than 80% of the inlet airflow into the ETC.

### **8.2 Handling of EUT and ETC**

#### **8.2.1 Selection and storage of EUT**

EUT shall be selected from normal manufactured batches or shall be a prototype that is representative for EUT from such batches. For determinations using the RAL-UZ 205 Option, EUT shall be stored in its original packaging in a standard normal climate ( $23 \pm 2^\circ\text{C}$ ,  $50 \pm 5\%$  RH) and tests should be executed within 10 working days after delivery of the EUT.

### 8.2.2 Loading Factor

To ensure detection of a minimum emission within a practicable time, the ETC with capabilities as specified in [Clause 7](#) shall be selected such that the [loading factor](#) is in the range of 1:4 to 1:400. For the ETC where the loading factor is in the range of 1:100 to 1:400, the air volume flow of the ETC shall be  $\leq 5 \text{ m}^3/\text{h}$ .

### 8.2.3 ETC purging

The selected ETC shall be unloaded and its interior walls shall be cleaned as described in ISO 16000-9.

The ozone half-life, the period of time for the ozone concentration (C) to drop from C to C/2, shall be greater than 10 minutes, when  $n = 1$ .

To determine the ozone half-life, the ETC should be deactivated by exposure to an ozone concentration of  $0,2 \text{ mg/m}^3$  to  $0,4 \text{ mg/m}^3$  for at least ten minutes or until a stable concentration is reached.

Thereafter, the ETC shall be purged with 4 ETC volumes of clean air.

### 8.2.4 Background concentrations ( $C_{bg}$ )

Following purging, the  $C_{bg}$  of [analyte](#) in the unloaded ETC shall be determined and recorded.

NOTE  $C_{bg}$  may stem from e.g. emissions from the ETC itself and sampling tubes or filters.

The  $C_{bg}$  values at  $n = 1$ , shall be below the limits in Table 1.

**Table 1 — Background concentrations**

Analyte	Limit
VOC and carbonyl compounds	$2 [\mu\text{g/m}^3]$ for any analysed substance
TVOC	$20 [\mu\text{g/m}^3]$
Ozone	$4 [\mu\text{g/m}^3]$
PM	$10 [\mu\text{g/m}^3]$
FP and UFP	$C_{pbg} = 2000 [\text{cm}^{-3}]$

### 8.2.5 EUT unpacking

Emissions from packaging may influence measurements considerably; in addition packaging itself may emit VOCs that are not representative for EUTs in typical use. Therefore, the EUT to be tested shall be removed from the shipping containers and all protective shipping packaging such as spacers, film wrapping and any other shipping/packaging elements before preparation (as specified in 8.2.6).

NOTE After unpacking, installation (step 8.2.7) may precede the preparation step (8.2.6).

### 8.2.6 Preparation of the EUT before testing

A  $60 \text{ g/m}^2$  to  $80 \text{ g/m}^2$  A4 paper with water content between 3,8% and 5,6%, and printing the patterns as specified in [A.1](#) and [A.2](#) are appropriate for the following preparatory operation. The maximum duration of the operating phase shall be determined. Thereafter, lightness ( $L^*$ ) and colour values ( $L^*$ ,  $a^*$ ,  $b^*$ ), as appropriate shall be determined from the printouts according to CIE 15:2004.

Before testing the EUT may be used up to the duration of the MUT. The MUT (as duration of the total operating cycles) is 120 minutes.



One to two 10-minutes operating cycles outside or inside the ETC shall be performed at least one day before the UFP test in order to determine the print speed, to ensure the proper operation and to avoid influence on emissions due to unstable UFP emission which sometimes may occur in operation after long-term disuse of the EUT.

For the RAL-UZ 205 option one or two 10-minute operating cycles or at most 1200 printed pages are acceptable for the purpose of EUT function testing and measuring of print speed and no further preparation and/or usage shall be executed unless required due to malfunction of the EUT.

Treatment conditions shall be recorded in the test report.

### **8.2.7 EUT installation**

Before installation, the EUT shall have sufficient consumables to complete the operations. In case of paper consumables, 60 g/m<sup>2</sup> to 80 g/m<sup>2</sup> A4 paper with water content from 3,8% to 5,6% shall be used.

To avoid contamination, the powered-off EUT shall be installed in the middle of the ETC as fast as possible and all operators shall leave the ETC immediately thereafter.

The EUT shall remain powered-off until the emission test as specified in [8.2.8](#), requires the EUT to be powered-on.

For the determination of FP and UFP specified in [8.6](#) and/or for the RAL-UZ 205 Option the EUT shall be installed on the day before the emission test.

The ETC shall remain closed until all sampling and/or monitoring is completed.

The installation date and time shall be recorded.

Emission testing, as specified in 8.2.6, shall not begin within at least 3 air exchanges following installation.

### **8.2.8 EUT operation during test**

#### **8.2.8.1 General**

VOC and carbonyl compounds as specified in [8.3](#); ozone as specified in [8.4](#); particulate matter as specified in [8.5](#) and FP and UFP as specified in [8.6](#) shall be determined while the EUT being controlled from outside the ETC.

#### **8.2.8.2 Special requirements on relative humidity**

To avoid condensation due to vaporisation of water from paper during the operating phase, incoming air with RH of at most 10% may be inserted in the ETC before the operating phase. In addition, the air exchange rate (n) may have to be increased to avoid such condensation. Increase of humidity during the operating phase also depends on the ETC volume. Condensation of water vapour (i.e. RH > 85%) on the ETC walls invalidates the test.

#### **8.2.8.3 Pre-operating phase**

To enter the pre-operating phase, the EUT shall be powered-on and remain in this phase between 1 and 4 air exchanges. For the determination of FP and UFP as specified in [8.6](#), particle counting shall be started from the start of the pre-operating phase because particle emission is observed for some EUTs soon after they are powered-on.

For the RAL-UZ 205 Option an air exchange rate of  $n = 1/h$  should be adjusted in the chambers. The pre-operating phase continues for a period of one air exchange.

#### **8.2.8.4 Operating phase**

The [Hard Copy Device](#) class of EUT shall operate at nominal speed. Operating may include monochrome, colour, single sided (simplex) and/or double sided (duplex) printing. The monochrome and colour print patterns specified in Annex A.1 and A.2 respectively shall be used for EUT using paper consumables.

Enter the operating phase by starting copying or printing. The output of the first printed page marks the start of the operating phase. It ends with the output of the last printed page.

In conjunction with other parameters such as n, ETC volume and the use of a post-operating phase, the duration shall be such that quantitative analysis is ensured.

The duration of the operating phase shall be planned as follows:

First priority: The duration shall be at least 10 minutes.

Second priority: If 10 minutes duration is technically not feasible the operational phase shall be as long as possible. The number of printed pages should not fall below 150. The maximum duration possible and the number of printed pages have to be checked prior to testing and have to be documented in the test protocol.

For the RAL-UZ 205 Option a device shall be tested with a configuration that allows a 10-minute printing time in simplex mode (single sided pages). For devices which cannot achieve a printing time of at least 5 minutes and cannot be equipped with large paper output trays due to design, the test shall be carried out in duplex mode (double sided printing). The devices shall be tested with default setting (standard print quality).

#### **8.2.8.5 Post-operating phase**

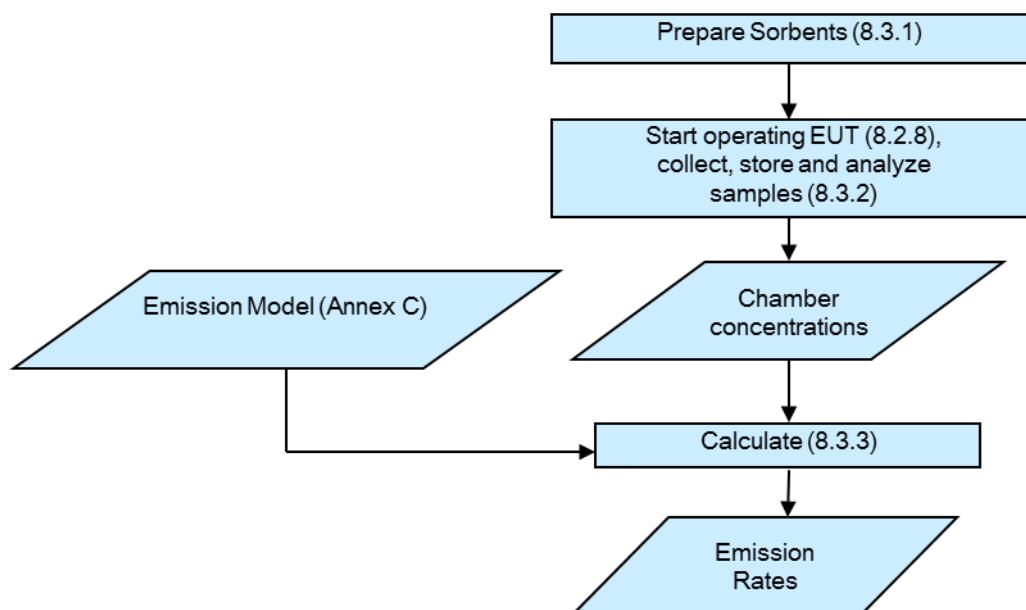
The post-operating phase starts when the operating phase ends, and may last up to four air exchanges.

#### **8.2.8.6 Recording of EUT operation**

The start and duration of the pre-operating, operating and post-operating phases shall be recorded.

### **8.3 VOC, carbonyl compounds**

The flow chart in Figure 2 illustrates the determination method for VOC, carbonyl compounds.



**Figure 2 — Determination method for VOC, carbonyl compounds**

### 8.3.1 Sorbents

VOC sampling and analysis shall be performed using the sorbents as specified in ISO 16017-1, with the exception of Chromosorb and PoraPak due to their high blank values: Tenax TA™ shall be conditioned and analysed according to ISO 16000-6 to minimise the production of artefacts, especially benzene.

For the RAL-UZ 205 Option Tenax tubes shall be spiked with an internal standard such as cyclodecane or deuterated toluene.

For carbonyl compounds, DNPH cartridges shall be used as sorbent material.

### 8.3.2 Sample collection

For VOC, duplicate samples shall be taken, and for carbonyl compounds at least one sample shall be taken.

Individual VOCs, carbonyl compounds with a concentration  $\geq 1,0 \mu\text{g}/\text{m}^3$  and, under the RAL-UZ 205 Option, benzene with a concentration  $\geq 0,25 \mu\text{g}/\text{m}^3$ , shall be detected.

In addition, Carbonyl compounds sampling shall be conducted as specified in ISO 16000-3.

Sampling shall be performed during:

- The [pre-operating](#) phase, starting at the beginning of this phase, or, under the RAL-UZ 205 Option, with a sample flow of 100 to 200 ml/min, from 20 minutes before the end until the end of the one-hour pre-operating phase; and
- The [operating](#) phase, starting at beginning of this phase, and may continue into the post-operating phase. Under the RAL-UZ 205 Option, sampling shall continue for one air exchange in the post-operating phase, with a sample flow of 100 to 200 ml/min.

Loaded samples shall be stored and analysed as specified in ISO 16000-3 and ISO 16000-6.

Identified VOCs shall be quantified using absolute response factors, determined by calibration. Unidentified VOCs shall be quantified using the toluene equivalents as a relative response factor.

When benzene is detected, this shall be verified and quantified by analysing a sample on alternate carbonaceous sorbent such as Carbotrap/Carbopack type materials.

When in doubt, positive findings of benzene are to be verified via a second independent sampling (e.g. using Carbotrap/Carbopack™ or activated carbon type materials).

### 8.3.3 Emission rate calculation

#### 8.3.3.1 General

This Clause specifies formulae that apply to practical situations that are special cases of the general case (as developed in Annex C).

Concentrations shall be determined, using the following equations:

$$C_s = \frac{m_s}{V_s} \quad C_{ope} = \frac{m_{ope}}{V_{ope}} \quad C_{pre} = \frac{m_{pre}}{V_{pre}} \quad C_{bg} = \frac{m_{bg}}{V_{bg}} \quad (1)$$

The Background emission rates are:

$$SER_{bg} = C_{bg} \cdot n \cdot V \quad (2)$$

#### 8.3.3.2 Emissions in the pre-operating phase

Assuming constant emission rates during the pre-operating phase, emission rates shall be calculated as follows.

##### a) If a sample is taken from the beginning of this phase:

$$SER_{pre} = \frac{(C_{pre} - C_{bg}) \cdot n^2 \cdot V \cdot t_{pre}}{\exp(-n \cdot t_{pre}) - 1 + n \cdot t_{pre}} \quad (3)$$

##### b) RAL-UZ 205 Option

$$SER_{pre} = C_{pre} \cdot n \cdot V \quad (4)$$

#### 8.3.3.3 Emissions in the operating and post-operating phase

##### 8.3.3.3.1 General case

Emission rates in these phases shall be determined using the following general formula:

$$SER_{ope} = \frac{(C_{ope} - C_{bg}) \cdot n^2 \cdot V \cdot t_G - SER_{pre} [\exp(-n \cdot (t_G - t_{ope})) + n \cdot (t_G - t_{ope}) - 1 + (1 - \exp(-n \cdot t_{pre})) \cdot (1 - \exp(-n \cdot t_G))]}{\exp(-n \cdot t_G) - \exp[-n \cdot (t_G - t_{ope})] + n \cdot t_{ope}} \quad (5)$$

### 8.3.3.3.2 Special cases

Consult Annex C for more detail on special cases.

If there is no post-operating phase ( $t_G = t_{ope}$ ), then:

$$SER_{ope} = \frac{(C_{ope} - C_{bg}) \cdot n^2 \cdot V \cdot t_G - SER_{pre} [(1 - \exp(-n \cdot t_{pre})) \cdot (1 - \exp(-n \cdot t_G))]}{\exp(-n \cdot t_G) - 1 + n \cdot t_G} \quad (6)$$

If the post-operating phase is relatively long ( $n \cdot t_G \geq 3$ ):

$$SER_{ope} = \frac{(C_{ope} - C_{bg}) \cdot n^2 \cdot V \cdot t_G - SER_{pre} [n \cdot t_G - \exp(-n \cdot t_{pre})]}{n \cdot t_{ope}} \quad (7)$$

### 8.3.3.3.3 RAL-UZ 205 Option

For the RAL-UZ 205 Option the post-operating phase shall last one air exchange and the following approximate formula shall be used for the calculation of  $SER_{ope}$  (i.e. (C.28) as derived in C.9):

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} \cdot n \cdot t_G}{\exp(-n \cdot t_G) - \exp[-n \cdot (t_G - t_{ope})] + n \cdot t_{ope}} \quad (8)$$

### 8.3.3.4 TVOC (RAL-UZ 205 Option)

The total VOC emission rate shall be calculated as the sum of all identified and unidentified substances with calculated emission rates equal to or larger than the following values:

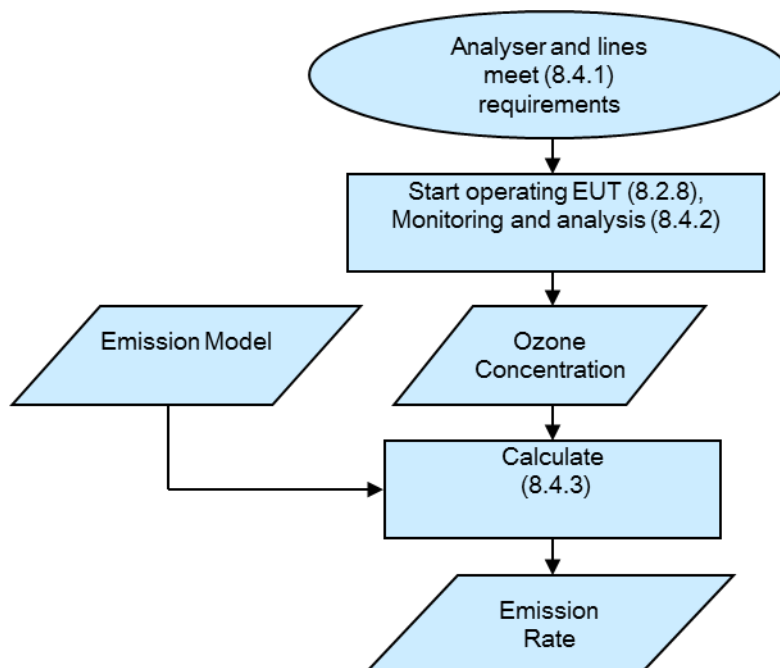
- For measurements in ETCs  $\leq 5 \text{ m}^3$ :  $SER_{pre} \geq 0,005 \text{ mg/h}$  and  $SER_{ope} \geq 0,05 \text{ mg/h}$ ;
- For measurements in ETCs  $> 5 \text{ m}^3$ :  $SER_{pre} \geq 0,010 \text{ mg/h}$  and  $SER_{ope} \geq 0,10 \text{ mg/h}$ .

Emission rates should - according to DIN 1333:1992-02 - be rounded to 3 or 2 decimal places for the pre-operating phase and the operating phase respectively.

The concentrations to be used in the subsequent calculations should be determined by subtracting the corresponding blank values from the measured values.

## 8.4 Ozone

The flowchart in Figure 3 illustrates the determination method for ozone.



**Figure 3 — Determination method for ozone**

#### 8.4.1 Analyser and sampling line requirements

Ozone analysers shall at least fulfil the following requirements:

- The capability to detect concentrations between  $4 \mu\text{g}/\text{m}^3$  and  $1 \text{mg}/\text{m}^3$ ;
- A precision of  $2 \mu\text{g}/\text{m}^3$ ;
- A sampling rate (may be important for small ETCs) of  $\leq 2 \text{ l}/\text{min}$ .

Ozone concentrations of the data points used to determine the maximum  $\Delta\text{Co}_3$  shall not be rounded to the nearest whole ppb ( $1 \text{ ppb} = 1.963 \mu\text{g}/\text{m}^3$ ) by data processing of the analyser because rounding may cause errors in the determination of the  $\Delta\text{Co}_3$ .

To prevent loss of ozone in the sampling line, it shall be of minimum length, not exceeding 4 m, and made of a flexible inert material such as PTFE.

#### 8.4.2 Monitoring

Since ozone is an unstable molecule, it shall be monitored and analysed instantaneously at least each 20 seconds for at least the first 6 minutes of the operating phase to determine the maximum  $\Delta\text{Co}_3$  as specified in 8.4.3. In addition, data points before and/or after the first 6 minutes of the operating phase shall be recorded so that the averaged ozone concentration time series can be calculated as specified in 8.4.3.

For the RAL-UZ 205 Option, the ozone determination is performed from the beginning of the operating phase to the end of the operating phase. The concentration should be recorded at least every 30 seconds, preferably every 15 seconds.

### 8.4.3 Emission rate calculation

The ozone emission rate is derived from the increase in ozone concentration during the first in 6 minutes of the operating phase. In this part of the operating phase ozone loss by chemical reactions with air constituents and by discharge due to air exchange is comparatively small. Therefore, the increase of ozone concentration with time is approximated as linear.

By taking formula 10 in this part of the operating phase

$$\frac{\Delta m}{\Delta t} = \frac{\Delta c_{O_3} * V}{\Delta t} \quad (9)$$

$\Delta m$ : emitted ozone mass [mg]

$\Delta c_{O_3}$ : change of ozone concentration [mg/m<sup>3</sup>]

$\Delta t$ : time interval [min]

the emission rate of ozone shall be calculated by formula 10:

$$SER_{O_3} = \frac{\Delta c_{O_3} * V * p * 60}{\Delta t * T * R} \quad (10)$$

A time interval  $\Delta t$  of two minutes and the maximum  $\Delta c_{O_3}$  shall be applied in formula 11. The data points recorded in 6 minutes from the start of the operating phase shall be used to determine the maximum  $\Delta c_{O_3}$ . This is the case when the averaged ozone concentration time series exhibits the greatest slope for the two minute time interval ( $c_{O_3}(t+2) - c_{O_3}(t) = \text{maximum}$ ). The averaged ozone concentration time series is created with the simple moving average over  $80 \pm 5$  seconds.

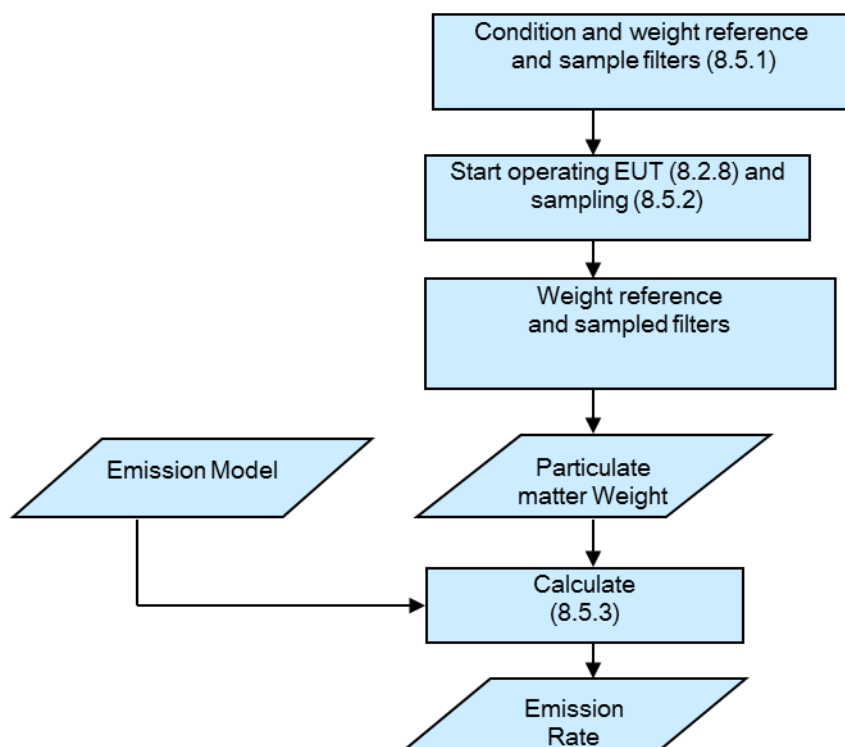
**NOTE** Theoretically, a time interval of the data points at the start of the operating phase gives the maximum  $\Delta m/\Delta t$  leading to the true emission rate. However, deviations of measured ozone concentration curves from the theoretical curve occur due to fluctuations of ozone data caused by incompleteness of air mixing in the chamber and effects of electric noises of ozone analysers, especially in larger chambers. The deviations make it difficult to determine an ozone emission rate according to the theory. Effects of electric noises can be reduced significantly by using the averaged ozone concentration time series. In addition,  $\Delta t$  of 2 minutes is selected and the determination of the maximum  $\Delta c_{O_3}$  for 6 minutes is conducted to minimize the effects of remaining fluctuations.

For analysers indicating values that are converted for the Standard Ambient Temperature and Pressure (SATP) of  $(273 + 25 = 298)$  K and 101 325 Pa (i.e. 1 atmosphere),  $SER_{O_3}$  shall be calculated using the actual ETC pressure ( $p$  in Pa), the actual ETC temperature ( $T$  in K) and the gas conversion constant ( $R = 339,8$  Pa/K), otherwise  $p/TR = 1$  shall be used:

**NOTE** If the temperature and pressure in the ETC equal the SATP,  $p/TR$  is 1.

## 8.5 Particulate matter

The flowchart in Figure 4 illustrates the gravimetric determination method for particulate matter emitted from EUT using consumables.



**Figure 4 — Determination method for particulate matter**

### 8.5.1 Weighing and Filter conditioning

The analytical balance, with a weighing precision of  $1\mu\text{g}$  or better, shall be located in a temperature and humidity controlled room (weighing room) as specified in [8.1.1](#).

Glass fibre filters with  $0,7\ \mu\text{m}$  pore size, or equivalent e.g.  $0,8\ \mu\text{m}$  pore size PVC filters, shall be used.

The filters shall be conditioned (remain in the weighing room) for at least 48 hours or to constant mass in the weighing room. Since even the smallest inevitable fluctuations in the relative humidity in the weighing room affect the weight of the glass fibre filter, at least one unloaded reference filter is weighed at the same time as the sampling filter before and after particulate matter sampling to minimise the influence of climate on the filter material by a climate correction. The unloaded reference filter and the sampling filters shall be weighed before sampling giving  $m_{\text{ref-before}}$  and  $m_{\text{before}}$ .

During particulate matter sampling, air is drawn through the test filter. As the relative humidity of this air may differ from that in the weighing room, the sampling filter must be conditioned again after particulate matter sampling for at least 48 hours or to a constant weight in the controlled room.

The reference filter is left in the weighing room constantly.

### 8.5.2 Sampling

Particulate matter shall be sampled during the operating and post-operating phases of the EUT. Sampling duration shall ensure the detection of at least  $5\ \mu\text{g}/\text{m}^3$  of particulate matter.

For the RAL-UZ 205 Option particulate matter sampling can be finalized after two air exchange periods of the post-operating phase.



### 8.5.3 Emission rate calculation

The unused reference filter and the sampling filters shall be weighted after sampling giving  $m_{\text{ref-after}}$  and  $m_{\text{after}}$ .

The particulate matter mass shall be corrected with the reference filter mass difference:

$$m_{\text{pm}} = (m_{\text{after}} - m_{\text{before}}) - (m_{\text{ref-after}} - m_{\text{ref-before}}). \quad (11)$$

With  $C_{\text{ope}} = m_{\text{pm}} / V_{\text{ope}}$ , the  $SER_{\text{pm}}$  shall be calculated using the following formula:

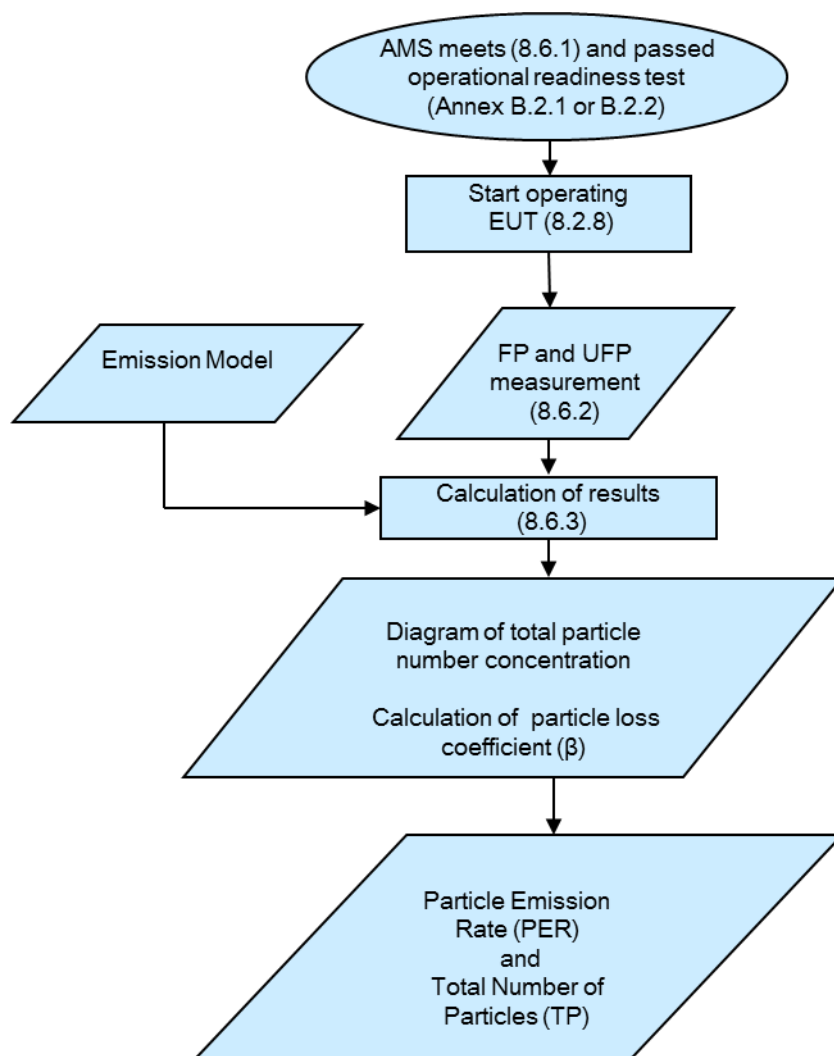
$$SER_{\text{pm}} = \frac{C_{\text{ope}} \cdot n^2 \cdot V \cdot t_G}{\exp(-n \cdot t_G) - \exp[-n \cdot (t_G - t_{\text{ope}})] + n \cdot t_{\text{ope}}} \quad (12)$$

For the RAL-UZ 205 Option the following approximate formula shall be used:

$$SER_{\text{pm}} = \frac{C_{\text{ope}} \cdot n \cdot V \cdot t_G}{t_{\text{ope}}} \quad (13)$$

## 8.6 Fine and Ultrafine Particles (FP and UFP)

The flow chart in Figure 5 illustrates the determination method for FP and UFP. FP and UFP determination does not substitute the gravimetric determination of particulate matter (8.5). It is an additional test to be performed in parallel.



**Figure 5 — Determination method for FP and UFP emissions**

## **8.6.1 General Requirements for Aerosol Measuring Systems (AMS)**

### **8.6.1.1 General**

An AMS shall be capable to measure the time dependent total particle number concentration with particle size range as specified in 8.6.1.2, particle number concentration range as specified in 8.6.1.3 and time resolution as specified in 8.6.1.4.

The operational readiness test for AMS shall be passed prior to testing as specified in [Annex B](#).

For the RAL-UZ 205 Option each individual AMS used must be qualified and approved as specified therein.

### **8.6.1.2 Particle size range**

The following instrument settings should be regarded as minimum requirements: The AMS shall be capable to count particles within a size range from at least 7 nm to at least 300 nm.

The detection efficiency at the lower size limit (7 nm) must be equal or higher than 50%.

NOTE Consult the AMS instruction manual for specific details.

#### **8.6.1.3 Particle number concentration range**

The below instrument criteria should be fulfilled without the application of an aerosol dilution system between the ETC sampling port and the inlet of the AMS.

CPC:

The required lower particle number concentration level shall be  $1 \text{ cm}^{-3}$  within the above specified size range.

The required upper particle number concentration level within the above specified size range shall be at least  $10^7 \text{ cm}^{-3}$ . It may be necessary to use a calibrated aerosol dilution stage with a specified dilution factor.

Fast AMS:

The required lower concentration level in the size channel nearest to the lower particle size limit of 7 nm shall be equal or lower than  $5000 \text{ cm}^{-3}$ .

The required upper concentration level in the size channel nearest to the upper particle size limit of 300 nm shall be equal or higher than  $10^6 \text{ cm}^{-3}$ .

NOTE 1 These requirements refer to concentration values normalized to size channels widths and a time resolution of 1 s.

NOTE 2 Refer to Annex B.1 for further information.

#### **8.6.1.4 Time resolution**

Particle number concentration values shall be recorded at a rate of at least 0.5 Hz.

#### **8.6.1.5 Working fluids for CPC**

CPCs shall be operated with the working fluids butanol or isopropanol.

NOTE CPCs which use water as a working fluid give much different  $C_p$ 's from those determined with other compliant CPCs for the purpose of this document.

#### **8.6.1.6 Connection of AMS to ETC**

The tubing between the ETC sampling port and the aerosol inlet of the AMS shall consist of electrically conductive material (e.g. conductive silicon rubber) and shall not exceed 3 m in length. Sharp bends in the tubing shall be avoided. The connecting hose should protrude at least 10 cm deep into the ETC.

#### **8.6.1.7 Quality Assurance**

AMS shall have the following capabilities:

- device-side controlled flow rates
- automatic display of malfunctions during measurement
- export of measurement data for evaluation
- display of the individual device settings to be selected by the user

- ability to adjust or synchronise time and date
- measurement of electrometer noise levels for fast AMS
- a detailed description of cleaning and maintenance procedures must be available.

### 8.6.2 Measurement

FP and UFP shall be measured during the pre-operating, operating and post-operating phases of the EUT. The result of FP and UFP measurement are presented as a diagram of  $C_p$  versus time comprising the period from 5 min before start of the operating phase to at least 30 min after its end.

### 8.6.3 Calculation

#### 8.6.3.1 General

The AMS manufacturer's software data display feature should be used in order to check the quality of measured data as described below.

- The particle number concentration time series should not reveal sudden discontinuities or steps during or after the operating phase. Occurring steps should not exceed a maximum acceptable step height of approximately  $15.000 \text{ cm}^{-3}$ .
- If this criterion cannot be met even after repeated measurement dilution of the aerosol between the ETC sampling port and the inlet of the AMS is acceptable in order to operate a CPC in single counting mode.

Technical note on steps in measured data from CPC: At low concentrations CPCs operate in the Single Counting Mode (SCM). With increasing particle number concentration the CPC switches to Photometric Mode (PM). Refer to the manufacturer's manual for the respective concentration range. For many CPCs it is typically between  $10.000$  and  $50.000 \text{ cm}^{-3}$ . In this range steps or discontinuities may occur.<sup>1</sup>

The AMS manufacturer's software should be used to export the total particle number concentration time series from the measuring file to an editable file. The data should be corrected accordingly if aerosol dilution was applied.

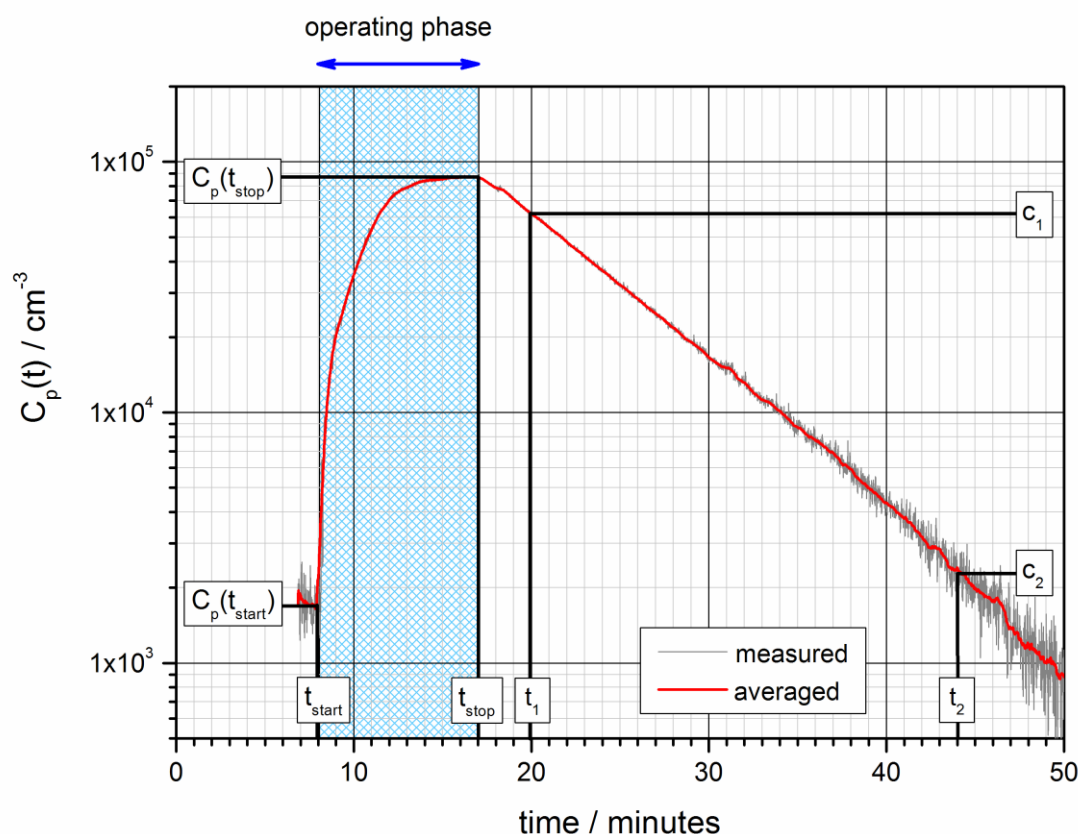
The averaged concentration time series, i.e. the Simple Moving Average over  $31 \pm 3$  seconds, shall be used to calculate the Particle loss coefficient  $\beta$ , the Particle Emission Rate PER and the Total number of emitted Particles TP.

#### 8.6.3.2 Calculation of Particle loss coefficient $\beta$

It is recommended to use consistent data formats and unit for time data points throughout the calculations.

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<sup>1</sup> GILHAM R.J.J., QUINCEY P.G., *Measurement and mitigation of response discontinuities of a widely used condensation particle counter*, J Aerosol Sci, Volume 40, Issue 7, July 2009, p 633-637)



**Figure 6 — Diagram of a total particle number concentration time series (example)**

- Plot the averaged concentration time series as shown in Figure 6 about 5 minutes before the operating phase, during the operating phase and at least for 30 minutes thereafter (optionally the concentration time series may be added to the diagram).
- As indicated in Figure 6, the value pairs  $c_1$ ,  $t_1$  and  $c_2$ ,  $t_2$  should be read from the smoothed time-dependent curve of particle number concentration as accurately as possible or determined by means of a cursor. On a logarithmic scale,  $t_1$  should be chosen within the linear descending range at least 5 minutes after the end of the operating phase and  $t_2$  at least 25 minutes after  $t_1$ .
- Calculate  $\beta$  using the following formula:

$$\beta = \frac{\ln\left(\frac{c_1}{c_2}\right)}{t_2 - t_1} \quad (14)$$

NOTE Time difference  $t_2 - t_1$  must be calculated in the unit [s].

Alternatively  $\beta$  may be determined by fitting the total particle number concentration decay after the end of particle emission to a single-exponential decay function:

$$C_p = \alpha \cdot \exp(-\beta \cdot t) \quad (15)$$

The correlation coefficient shall be larger than 0.98 to ensure the quality of the following calculations.

### 8.6.3.3 Calculation of PER and TP

- a) The values  $t_{\text{start}}$  and  $C_p(t_{\text{start}})$  should be read from the smoothed time-dependent curve of particle number concentration (cf. Figure 6) as accurately as possible or determined by means of a cursor.
- b) The time difference  $\Delta t$  between two successive data points of the particle number concentration  $C_p(t)$  is given in the manufacturer's manual.

NOTE  $\Delta t$  must be given in the unit [s] and is generally set to 1 s

- c)  $PER(t)$  [ $s^{-1}$ ] will be calculated using  $\Delta t$ ,  $\beta$  and the data set of the smoothed particle number concentration.

$$PER(t) = V \left[ \frac{C_p(t) - C_p(t - \Delta t) \exp(-\beta \cdot \Delta t)}{\Delta t \exp(-\beta \cdot \Delta t)} \right] \quad (16)$$

$C_p(t)$ : smoothed curve of particle number concentration [ $cm^{-3}$ ]

$V$ : ETC volume [ $cm^3$ ]

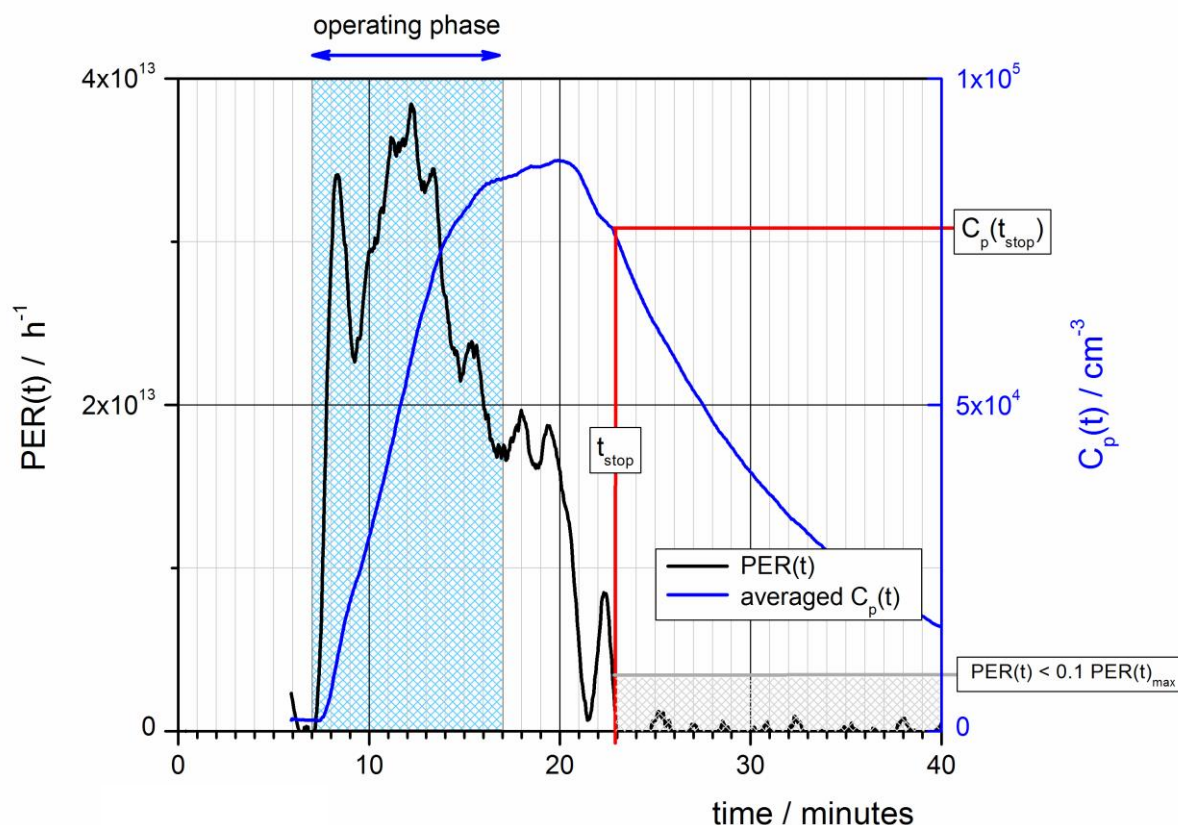
$\Delta t$ : time difference between two successive data points [s]

$\beta$ : particle loss coefficient [ $s^{-1}$ ]

NOTE  $C_p(t)$  is usually in the unit [ $cm^{-3}$ ]. The chamber volume  $V_c$  must be accordingly converted into the unit [ $cm^3$ ].  $\Delta t$  must be substituted in the unit [s].

$PER(t)$  and the smoothed  $C_p(t)$  curve will be plotted according to the example in Figure 7. The abscissa (time-axis) should be given in units of [min] or [s].

- d) Plot  $PER(t)$  as shown in Figure 7.



**Figure 7 — Diagram of PER(t) and  $C_p(t)$**

- e) The values  $t_{stop}$  and  $C_p(t_{stop})$  shall be read with high accuracy from the averaged concentration time series curve in Figure 7 as indicated.  $t_{stop}$  marks the point on the time axis, from which on PER(t) remains below 10% of its maximum.

**NOTE** In some cases the particle emission rate curve may partially fall below the zero baselines due to particle concentration reduction effects in the ETC, not considered in the calculations. Before and after the particle emission the PER(t) values shall be near to the zero baseline, i.e. they shall deviate by less than  $\pm 5\%$  of the PER(t)-maximum from zero.

- f) Proceed with final steps in 8.6.3.3.4.

#### 8.6.3.4 Calculation of PER and TP, final steps

- a) The difference of total particle number concentrations ( $\Delta C_p$ ) shall be calculated as follows:

$$\Delta C_p = C_p(t_{stop}) - C_p(t_{start}) \quad (17)$$

- b) The arithmetic mean of measured concentration values between  $t_{start}$  and  $t_{stop}$  shall be calculated:

$$C_{av} = \frac{\sum_{i=1}^n C_{p,i}}{n} \quad (18)$$

with  $n$ : number of measured concentration values between  $t_{start}$  and  $t_{stop}$ .

- c) PER shall be calculated using the following formula:

$$PER = V \left( \frac{\Delta C_p}{t_{stop} - t_{start}} + \beta \cdot C_{av} \right) \quad (19)$$

Assume 25% as relative error of PER [h<sup>-1</sup>]

NOTE  $\Delta C_p$  and  $C_{av}$  have the unit [cm<sup>-3</sup>].  $\beta$  is defined in the unit [s<sup>-1</sup>]. For the correct application of the formula, the chamber volume  $V$  must be substituted in the unit [cm<sup>3</sup>] and the emission time  $t_{stop} - t_{start}$  in the unit [s].

- d) TP shall be calculated using the following formula:

$$TP = PER \cdot (t_{stop} - t_{start}) \quad (20)$$

Assume 25% as relative error of TP.

The calculation of PER and TP is not reliable if:

$$\Delta C_p \leq 1000 \text{ cm}^{-3}$$

In this case, the numeric results ( $\beta$ , PER, TP) shall be specified in the protocol as “not quantifiable”.

- e) For the RAL-UZ 205 Option the standard particle emission rate  $PER_{10}$  for an operating phase of 10 minutes (i.e. 600 seconds) shall be calculated using the following formula.

$$PER_{10} = TP \cdot \frac{600}{t_{ope}} \quad (21)$$

The length of the operating phase  $t_{ope}$  must be substituted in the unit [s].

## 9 Test report

The test report shall include the following, if applicable and available:

### Test laboratory

- Reference to ISO/IEC 28360.
- Name and address of test laboratory.
- Name of the responsible person.
- Unique identification number of the test report.

### EUT description

- Manufacturer.
- Type, brand name and serial number of EUT, and if tabletop or floor-mounted.
- Print or copying speed according to manufacturer's information.
- Identification number (model number) and lot number of consumables used.



- History of the EUT and of the consumables (date of production, date of arrival to the test laboratory, date and time of unpacking, storage time, environmental storing conditions before test).
- Types of packaging.
- External dimensions.
- Number of hours the equipment has been used while energised during manufacture and testing.

#### **Test conditions and methods**

- Date of test.
- Description of the test apparatus and methods used (ETC, clean air system, environmental control system, sample collection, analytical instrumentation, standard generation and calibration).
- Description of AMS:
  - Manufacturer, model, type and serial number of AMS
  - Name and version of the AMS software
  - Date of last calibration and /or maintenance
  - AMS settings used for measurement
  - Particle size range (or Fast AMS: Particle size range and number of channels within this range)
  - Result of the mandatory operational readiness test (see Annex B).
- Statement on the compliance to Quality Assurance items.
- Name and storage location of the raw data measurement files.
- Name and storage location of the ASCII-export data files.
- ETC test conditions (T, RH, n).
- Background concentrations ( $C_{bg}$ ).
- Loading factor.
- Sampling methods used (sorbent(s) used, volume sampled, sampling start time and duration).
- Start and duration of pre-operating, operating and post-operating phases.
- Test specification for intended functions.
- Print speed during test and number of printed pages.
- Print mode used for testing (monochrome or colour; simplex or duplex).
- Lightness and/or colour values ( $L^*$ ,  $a^*$ ,  $b^*$ ) from printout.
- Ozone half-life of the unloaded ETC.
- Detection limits of VOC, carbonyl compounds, ozone and particulate matter.
- Disturbances of - and deviations from test methods.

### **Emission rate determination and total number of particles determination**

- Identification of the formulae used to determine specific emission rates from measured ETC concentrations.
- Identification of the calculation method used to determine PER and TP.

### **Results**

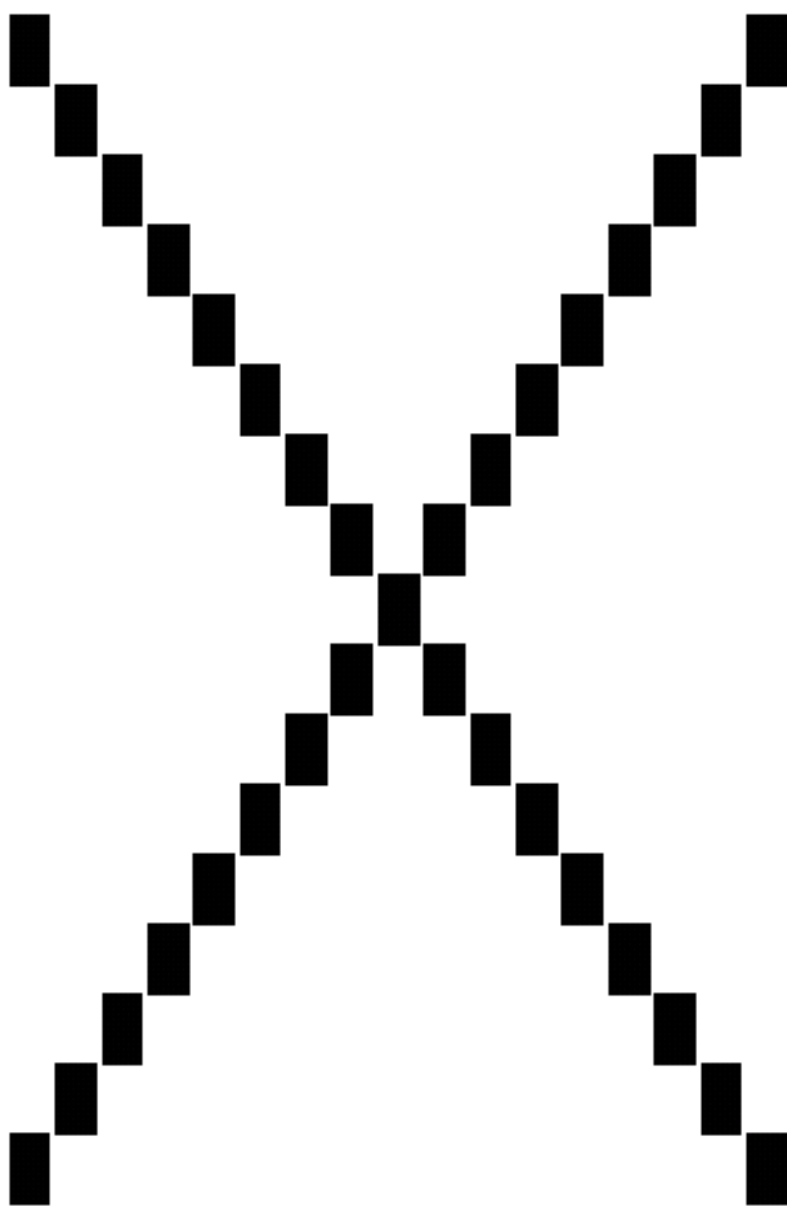
- Name, CAS-number and concentration of identified VOCs, formaldehyde and other carbonyl compounds in pre-operating phase and operating phase and calculated emission rates.
- Concentration of unidentified VOCs in pre-operating phase and operating phase and calculated emission rates.
- Total VOC value as the sum of the quantified and unidentified compounds during pre-operating phase and operating phase as well as calculated emission rates for the RAL-UZ 205 Option.
- Maximum change of ozone concentration for 2 minutes and calculated ozone emission rate.
- Mass of sampled particulate matter ( $m_{pm}$ ) and calculated emission rate ( $SER_{pm}$ ).
- Diagram of particle number concentration time series as specified.
- Dilution factor if aerosol dilution was applied.
- Calculated Particle loss coefficient  $\beta$ .
- Particle emission rate PER.
- Total number of emitted particles TP.
- Standard particle emission rate  $PER_{10}$ , for the RAL-UZ 205 Option.

## **Annex A** **(normative)**

### **Print Patterns**

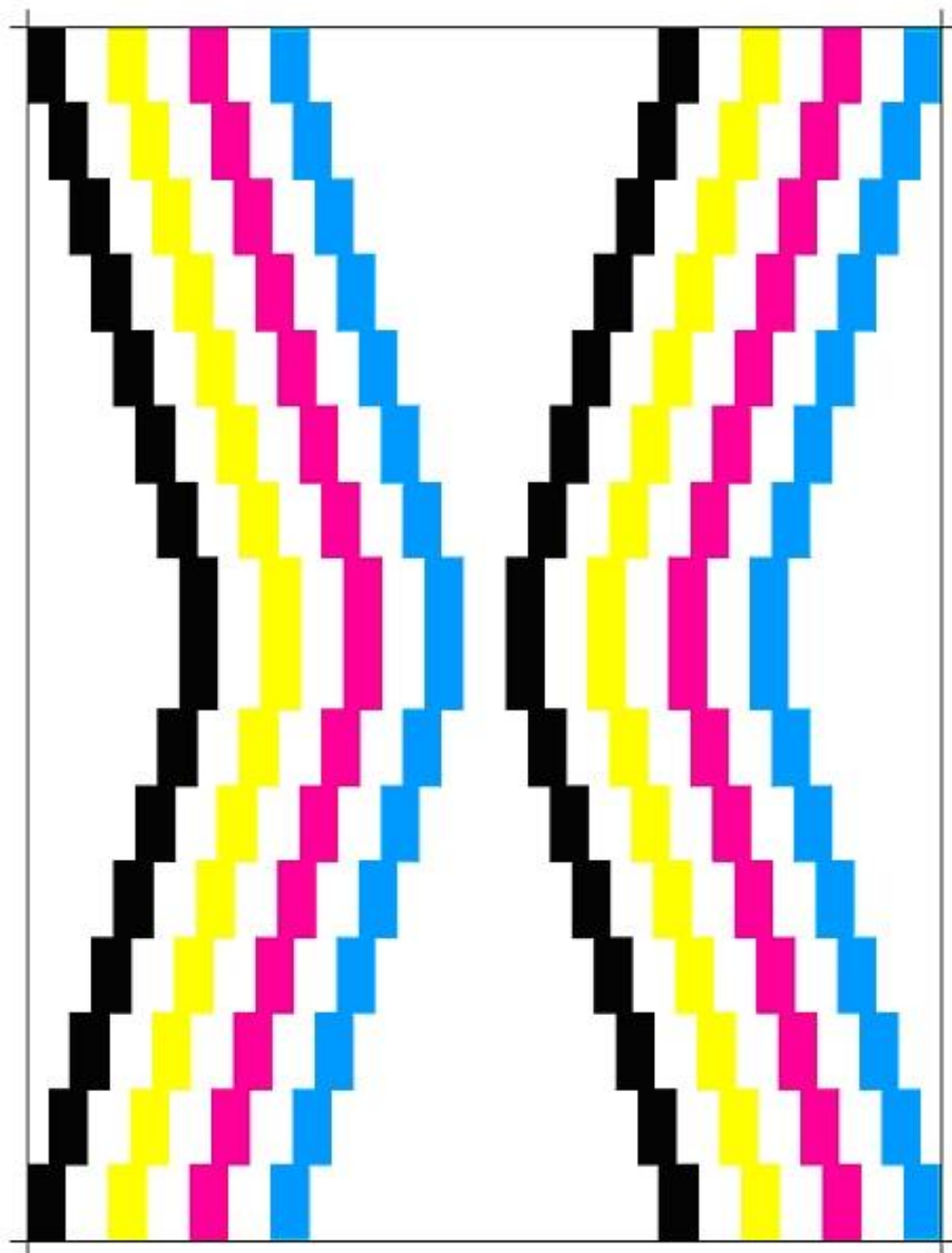
#### **A.1 Monochrome print pattern, 5% coverage**

This Annex illustrates the monochrome pattern with 5% black coverage; tests of EUT using paper consumables as specified in this document shall be executed using the pattern at <http://www.ecma-international.org/publications/standards/Ecma-328.htm>.



## A.2 Colour print pattern, 20% coverage

This Annex illustrates the colour pattern with 20% colour coverage (5% needed for each colour [black, magenta, cyan, yellow] tests of EUT using paper consumables as specified in this document shall be executed using the pattern at <http://www.ecma-international.org/publications/standards/Ecma-328.htm>.





## **Annex B** **(normative)**

### **Preparatory AMS Test Procedures**

#### **B.1 Procedures for operational readiness of AMS**

This Annex specifies procedures for testing the operational readiness of AMS. These steps are additional requirements to periodical instrument maintenance.

##### **B.1.1 Particle size concentration range measurements**

The lower particle size limit is the smallest diameter at which the counting efficiency of a specific AMS is 50%.

The upper particle size limit is the largest diameter at which the counting efficiency of a specific AMS is 50%.

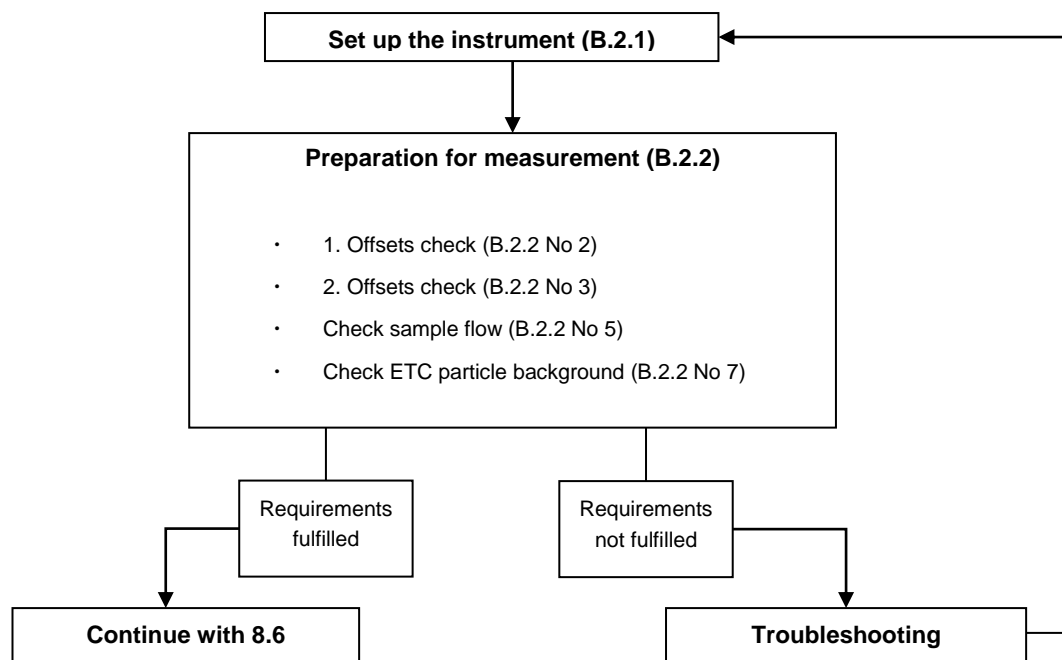
##### **B.1.2 Particle number concentration range measurements**

The lower particle number concentration level is the concentration that can be distinguished with a statistical certainty of 95% from the reported concentration background value due to the instrument's false count rate. The false count rate is the reported count rate which is not caused by particles.

For Fast AMS based on the measurement of electric currents the lower particle number concentration level decrease with increasing particle size while the upper particle number concentration level decreases with increasing particle size. Both limits are much higher compared to other AMS, such as CPCs.

The size dependent number concentration of Fast AMS may be presented as absolute concentration  $C_P$ , or as concentration normalized to the width of the respective size class  $dc_i/d\log d_i$ , where index  $i$  corresponds to the size class.

## B.2 Procedures for operational readiness test of Fast AMS



**Figure B.1 — Scheme for the operational readiness test for Fast AMS**

### B.2.1 Set up of instrument

1. Check for proper cleanliness of the instrument and tubing.
2. Set up the Fast AMS for the purpose of enabling a straight connection between the sampling port of the ETC and the aerosol inlet of the AMS with a maximum length of 3 m.
3. Check date and time settings of AMS and/or AMS software and laboratory clock and synchronize if date is different and/or if time differs by more than 1 s.

### B.2.2 Preparation for measurement

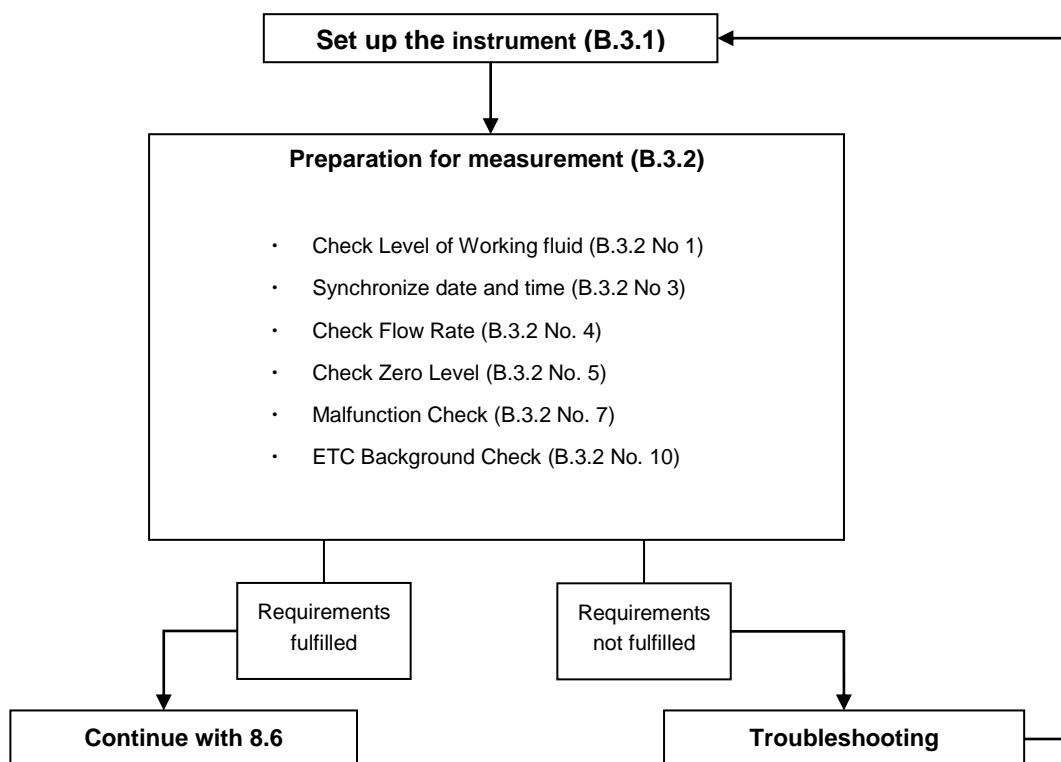
The following steps should be executed in sequence:

1. All operating parameters (air temperature, voltage, internal pressure and flow rates) are checked.
2. A reset (zeroing) is performed according to the manufacturer's instructions after instrument warmup (first check). Electrometer current offsets and RMS values will be recorded and checked for compliance with manufacturer's specifications.
3. After another period of 30 minutes, step 2 is repeated (second check). Electrometer offsets from first and second check may not differ by more than  $\pm 10$  fA. Compliance with this requirement is mandatory and must be stated in the test protocol. Instruments which do not pass this test need maintenance and may not be used for test purposes.
4. The HEPA filter is removed from the aerosol inlet of the AMS.



5. The sampling flow rate of the AMS is checked. An internal flow meter should preferably be used for this. Otherwise, an externally calibrated flow meter must be used. The measured flow rate of the AMS must not deviate by more than  $\pm 10\%$  of the specified set point in the calibration certificate.
6. The AMS is connected to the sampling port of the ETC.
7. The particle background concentration is measured in the ETC. The background concentration level should correspond to the value given in 8.2.4, Table 1.

### B.3 Procedures for operational readiness test of CPC



**Figure B.2 — Preparation scheme for CPC**

#### B.3.1 Set up the instrument

For the measurement of total particle number concentration, only those CPCs are used which use isopropanol or butanol as a working fluid. Check for proper cleanliness of the instrument and tubing.

Set up the CPC for the purpose of enabling a straight connection between the sampling port of the ETC and the aerosol inlet of the CPC with a maximum length of 3 m.

### B.3.2 Preparation for measurement

The following steps should be executed in sequence:

1. The work fluid reservoir of the CPC will be filled. If there is one - the excess reservoir of the CPC should be checked and emptied in order to avoid malfunctions during the measurements.
2. The CPC will be switched on and runs through warm-up according to the manufacturer's instructions.
3. Time and date of the CPC will be synchronized with a maximum deviation of 1 second to the laboratory timer.
4. CPC function test: The sampling flow rate of the CPC is checked. An internal flow meter should preferably be used for this. Otherwise, an externally calibrated flow meter must be used. The measured flow rate of the CPC must not deviate by more than  $\pm 10\%$  of the set point specified in the calibration certificate.
5. The inlet of the CPC will be connected to a HEPA filter (filter efficiency  $\geq 99.99\%$ ). If particle number concentrations  $> 1 \text{ cm}^{-3}$  are indicated over a period of 1 min - after any leaks between the HEPA filter and aerosol inlet were eliminated - there is a malfunction in the CPC.
6. The HEPA filter is removed from the aerosol inlet of the CPC.
7. The particle number concentration in ambient air outside the ETC is measured. Readings should exceed  $1 \text{ cm}^{-3}$ . Aerosol sources with sufficiently high output may be used for this test. A zero readout indicates a malfunction of the CPC.
8. The correct function of the CPC will be reported.
9. The CPC is connected to the sampling port of the ETC via a conductive material (e.g. conductive silicone tube, stainless steel) with a maximum length of 3 m.
10. The measured particle background concentration in the ETC must not exceed the specified values specified in 8.2.4, Table 1.

## Annex C (informative)

### Emission rate model

#### C.1 Objective

This Annex develops a generalised formula to calculate emission rates from VOC, carbonyl compounds and particulate matter concentrations sampled in an ETC.

NOTE This Annex has been developed with Hard Copy Devices in mind therefore “printing phase” denotes the operating phase.

#### C.2 Approach

By sampling over a period of time averaged concentrations are acquired.

Emission rates must be calculated from these average concentrations. The average concentrations during printing can be described by four different regions as shown in Figure C.1. During printing, there are two regions: m1 for printing, and m2 for the decay of the initial concentration ( $C_0$ ) built up during the pre-operating phase. m3 represents the concentration decay from  $C_{max}$  during the post-operating phase, and m4 is the concentration build-up during the post-operating phase from pre-operating and background emission.

The following is assumed:

- The emission rates are constant;
- The emission rates during pre- and post-operating phases are equal;
- No energy saving modes apply during the pre- and post-operating phase.

Cases, where the above assumptions do not apply, are outside the scope of this document.

#### C.3 General mass balance and concentration equations

The following mass balance is valid for an ETC containing an emission source with a SER:

$$\frac{dC}{dt} = \frac{SER}{V} - nC \quad (C.1)$$

Integrate (C.1) to obtain C:

$$C = \frac{SER}{n \cdot V} [1 - \exp(-n \cdot t)] + C_0 \exp(-n \cdot t) \quad (C.2)$$

## C.4 Background SER

With  $SER = SER_{bg}$  and  $C_o = 0$  in (C.2), the background concentration is:

$$C_{bg} = \frac{SER_{bg}}{n \cdot V} [1 - \exp(-n \cdot t)] \quad (C.3)$$

$$\text{For } n \cdot t \geq 3, (C.3) \text{ reduces to (equilibrium): } SER_{bg} = C_{bg} \cdot n \cdot V \quad (C.4)$$

To simplify,  $SER_{bg}$  may be substituted by  $C_{bg} \cdot n \cdot V$  (from C.4) in derived formulae below, as has been applied for the formulae in [Clause 8](#).

## C.5 Emission during pre-operating phase

Assume the emission model as shown in Figure C.1. During the pre-operating phase, there are two constant emission sources; one originates from the background of the ETC, and the other originates from the EUT in the pre-operating phase.

$SER = SER_{bg} + SER_{pre}$  in (C.1) yields:

$$\frac{dC}{dt} = \frac{SER_{bg} + SER_{pre}}{V} - nC \quad (C.5)$$

$$C_{pre} = \frac{SER_{bg} + SER_{pre}}{n \cdot V} [1 - \exp(-n \cdot t)] + C_o \exp(-n \cdot t) \quad (C.6)$$

Because the concentration at the beginning of the pre-operating phase ( $C_o$ ) equals the background concentration  $C_{bg}$ , (C.6) becomes:

$$C_{pre} = \frac{SER_{pre}}{n \cdot V} [1 - \exp(-n \cdot t)] + \frac{SER_{bg}}{n \cdot V} \quad (C.7)$$

The total measure for mass of sampled VOCs is equal to the product of the averaged concentration and sampling time ( $C_{pre} \cdot t_{pre}$ ), and can be obtained by integrating (C.7) from  $t=0$  to  $t=t_{pre}$ :

$$C_{pre} \cdot t_{pre} = \int_0^{t_{pre}} \left\{ \frac{SER_{pre}}{n \cdot V} [1 - \exp(-n \cdot t_{pre})] + \frac{SER_{bg}}{n \cdot V} \right\} dt = \frac{SER_{pre}}{n^2 \cdot V} [n \cdot t_{pre} + \exp(-n \cdot t_{pre}) - 1] + \frac{SER_{bg}}{n \cdot V} t_{pre} \quad (C.8)$$

Rearrange (C.8) for  $SER_{pre}$ :

$$SER_{pre} = \frac{C_{pre} \cdot n^2 \cdot V \cdot t_{pre} - SER_{bg} \cdot n \cdot t_{pre}}{n \cdot t_{pre} + \exp(-n \cdot t_{pre}) - 1} = \frac{(C_{pre} - C_{bg}) \cdot n^2 \cdot V \cdot t_{pre}}{n \cdot t_{pre} + \exp(-n \cdot t_{pre}) - 1} \quad (C.9)$$

## C.6 Emission during operating phase

During the operating phase the concentration build-up originates from EUT operation and the background concentration only.  $C_{ope}$ . Integration of (C.1) with  $SER = SER_{bg} + SER_{ope}$  yields:

$$C_{ope} = \frac{SER_{ope} + SER_{bg}}{n \cdot V} [1 - \exp(-n \cdot t)] + C_o \exp(-n \cdot t) \quad (C.10)$$

NOTE In (C.10)  $C_o$  is equal to the concentration at the end of the pre-operating phase ( $C_{pre}$ ) determined in (C.7).

In Figure C.1, the terms from m1 to m4 denote the product of average concentration, stemming from a source, and the time period of the phase under consideration. Integrating equation (C.10) over time from zero to the end of printing ( $t_{ope}$ ), yields m1 and m2.

$$m1 = \int_0^{t_{ope}} \frac{SER_{ope} + SER_{bg}}{n \cdot V} [1 - \exp(-n \cdot t)] dt = \frac{(SER_{ope} + SER_{bg}) \cdot [n \cdot t_{ope} + \exp(-n \cdot t_{ope}) - 1]}{n^2 \cdot V} \quad (C.11)$$

$$m2 = \int_0^{t_{ope}} [C_o \cdot \exp(-n \cdot t)] dt = \frac{C_o \cdot n \cdot V [1 - \exp(-n \cdot t_{ope})]}{n^2 \cdot V} \quad (C.12)$$

- m1: Concentration area over time during printing
- m2: Concentration area over time which decays from  $C_o$  due to air exchange
- m3: Concentration area over time which decays from  $C_{max}$  to the equilibrium concentration of pre-operating and background concentration
- m4: Concentration area over time during post-operating phase.

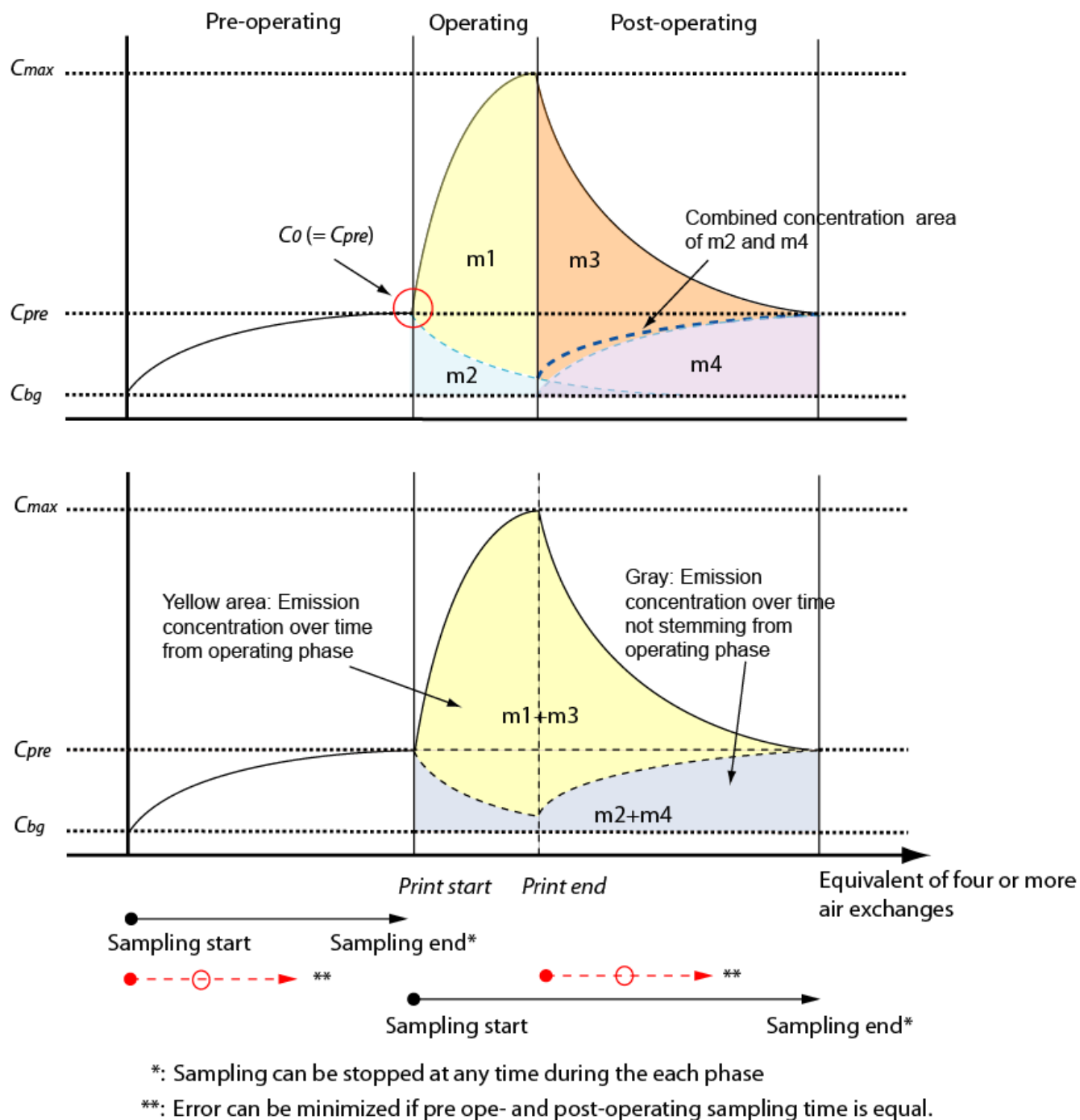


Figure C.1 — Representation of concentration change during printing and post operating phase

## C.7 Emission during post-operating phase

The concentration built-up from the operating phase ( $C_{max}$ ) decreases with the air exchange in the post-operating phase. But emissions from background level to the level at the end of the pre-operating phase increase. Obtain  $C_{max}$  in Figure C.1 from (C.10) for  $t = t_{ope}$ :

$$C_{max} = \frac{(SER_{ope} + SER_{bg})}{n \cdot V} [1 - \exp(-n \cdot t_{ope})] + Co \exp(-n \cdot t_{ope}) \quad (C.13)$$

Similar to (C.2), the concentration during the post-operating can be written as:

$$C_{post} = \underbrace{\frac{(SER_{pre} + SER_{bg})}{n \cdot V} [1 - \exp(-n \cdot (t - t_{ope}))]}_{\text{Term due to emissions in post operating phase}} + \underbrace{C_{max} \exp[-n \cdot (t - t_{ope})]}_{\text{Concentration reached at } C_{max} \text{ decreased by air exchange}} \quad (C.14)$$

$m_3$  in Figure C.1 is obtained by integrating the second term of (C.14) over time from  $t_{ope}$  to  $t_G$ :

$$\begin{aligned} m_3 &= \int_{t_{ope}}^{t_G} \left\{ \frac{(SER_{ope} + SER_{bg})}{n \cdot V} [1 - \exp(-n \cdot t_{ope})] + Co \exp(-n \cdot t_{ope}) \right\} \cdot \exp(-n \cdot (t - t_{ope})) dt \\ &= [\exp(-n(t_G - t_{ope})) - 1] \cdot \left\{ \frac{SER_{ope} + SER_{bg}}{n^2 \cdot V} [\exp(-n \cdot t_{ope}) - 1] - \frac{Co}{n} \exp(-n \cdot t_{ope}) \right\} \end{aligned} \quad (C.15)$$

Similarly,  $m_4$  can be found by integrating the first term of (C.14):

$$\begin{aligned} m_4 &= \int_{t_{ope}}^{t_G} \frac{(SER_{pre} + SER_{bg})}{n \cdot V} [1 - \exp(-n \cdot (t - t_{ope}))] dt \\ &= \frac{(SER_{pre} + SER_{bg})}{n^2 \cdot V} [n(t_G - t_{ope}) + \exp(-n(t_G - t_{ope})) - 1] \end{aligned} \quad (C.16)$$

The average concentration ( $C_{ope}$ ) during sampling in the operating and post-operating phase is:

$$C_{ope} = \frac{m_1 + m_2 + m_3 + m_4}{t_G} = \frac{m_{ope}}{V_{ope}} \quad (C.17)$$

Insert  $m_1$ ,  $m_2$ ,  $m_3$  and  $m_4$  in (C.11), (C.12), (C.15), and (C.16) to obtain  $C_{ope}$  and rearrange for  $SER_{ope}$ :

$$\begin{aligned} SER_{ope} &= \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} [\exp(-n(t_G - t_{ope})) + n(t_G - t_{ope}) - 1]}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \\ &\quad - \frac{SER_{bg} [\exp(-nt_G) + nt_G - 1] + Co \cdot n \cdot V [1 - \exp(-n \cdot t_G)]}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \end{aligned} \quad (C.18)$$

The initial concentration  $C_0$  can be determined from the emission during the pre-operating phase:

$$C_0 = \frac{SER_{pre}}{n \cdot V} [1 - \exp(-n \cdot t_{pre})] + \frac{SER_{bg}}{n \cdot V} \quad (C.19)$$

If the air exchange rates in the pre-operating and operating phase differ,  $n$  can be replaced by  $n_{pre}$ :

$$C_0 = \frac{SER_{pre}}{n_{pre} \cdot V} [1 - \exp(-n_{pre} \cdot t_{pre})] + \frac{SER_{bg}}{n_{pre} \cdot V} \quad (C.20)$$

(C.18) can be simplified using (C.19), where  $n$  is equal in the pre-, post- and operating phases:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} [\exp(-n(t_G - t_{ope})) + n(t_G - t_{ope}) - 1 + (1 - \exp(-n \cdot t_{pre})) \cdot (1 - \exp(-n \cdot t_G))] - SER_{bg} \cdot n \cdot t_G}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \quad (C.21)$$

(C.21) is the general case formula used in the main text.

**NOTE** It is advised to use the same sampling time during pre-operating ( $t_{pre}$ ) and post-operating ( $t_G - t_{ope}$ ) if the emission behaviour of the EUT is unknown (one or more energy modes in addition to save energy mode). In that case, (C.21) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} [n(t_G - t_{ope}) - \exp(-nt_G) + \exp(-n \cdot (2t_G - t_{ope}))] - SER_{bg} \cdot n \cdot t_G}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \quad (C.22)$$

## C.8 Special cases

**Case 1** Pre-operating phase is relatively long ( $nt_{pre} \geq 3$ ), and post-operating phase relatively long ( $nt_G \geq 3$ ), (C.21) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} \cdot [n(t_G - t_{ope}) - \exp(-n \cdot t_{pre})] - SER_{bg} \cdot n \cdot t_G}{nt_{ope}} \quad (C.23)$$

and if  $nt_{pre} \geq 3$ , (C.23) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} \cdot [n(t_G - t_{ope})] - SER_{bg} \cdot n \cdot t_G}{nt_{ope}} \quad (C.24)$$

and if background concentration is neglected, (C.24) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} \cdot [n \cdot (t_G - t_{ope})]}{nt_{ope}} \quad (C.25)$$



**Case 2** Pre-operating phase is relatively long ( $nt_{pre} \geq 3$ ), and the air exchange rate during the pre-operating and operating phases are equal ( $n_{pre}=n$ ), (C.21) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} [\exp(-n(t_G - t_{ope})) + n(t_G - t_{ope}) - \exp(-n \cdot t_G)] - SER_{bg} \cdot n \cdot t_G}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \quad (C.26)$$

## C.9 Model for RAL-UZ 205 Option

The model developed in earlier chapters of this Annex, and the model for the RAL-UZ 205 Option only differ by the definition of the emission rate during the operating phase.

The emission rate during the operating phase can be thought to be composed of  $SER_{ope}$  and  $SER_{pre}$ , as described in the following model.

Figure C.2a presents the situation where equilibrium has been reached in the pre-operating phase. In Figure C.2b no equilibrium has been reached in the pre-operating phase, but it is assumed that the EUT enters an energy save mode during the pre-operating phase, so that a quasi-equilibrium is attained at the end of the pre-operating phase.

Emission is defined as: the area under the concentration curve, expressed by  $m1' + m3'$  in Figure C.2, which can be seen as the increase in concentration due to printing.

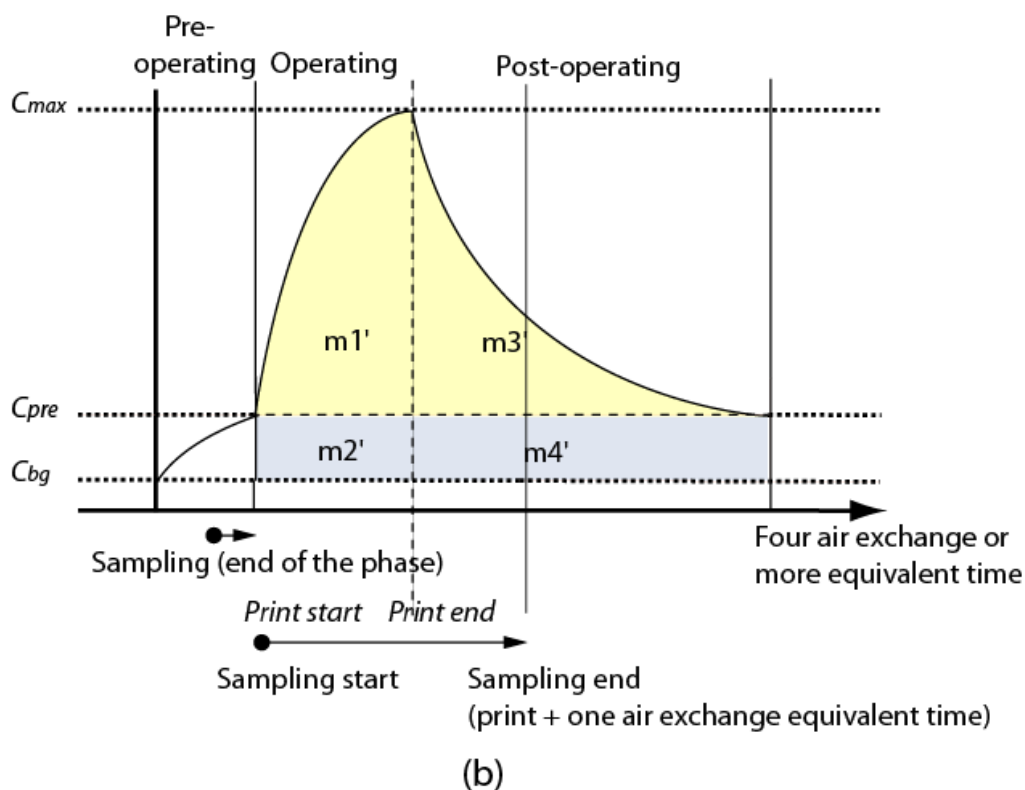
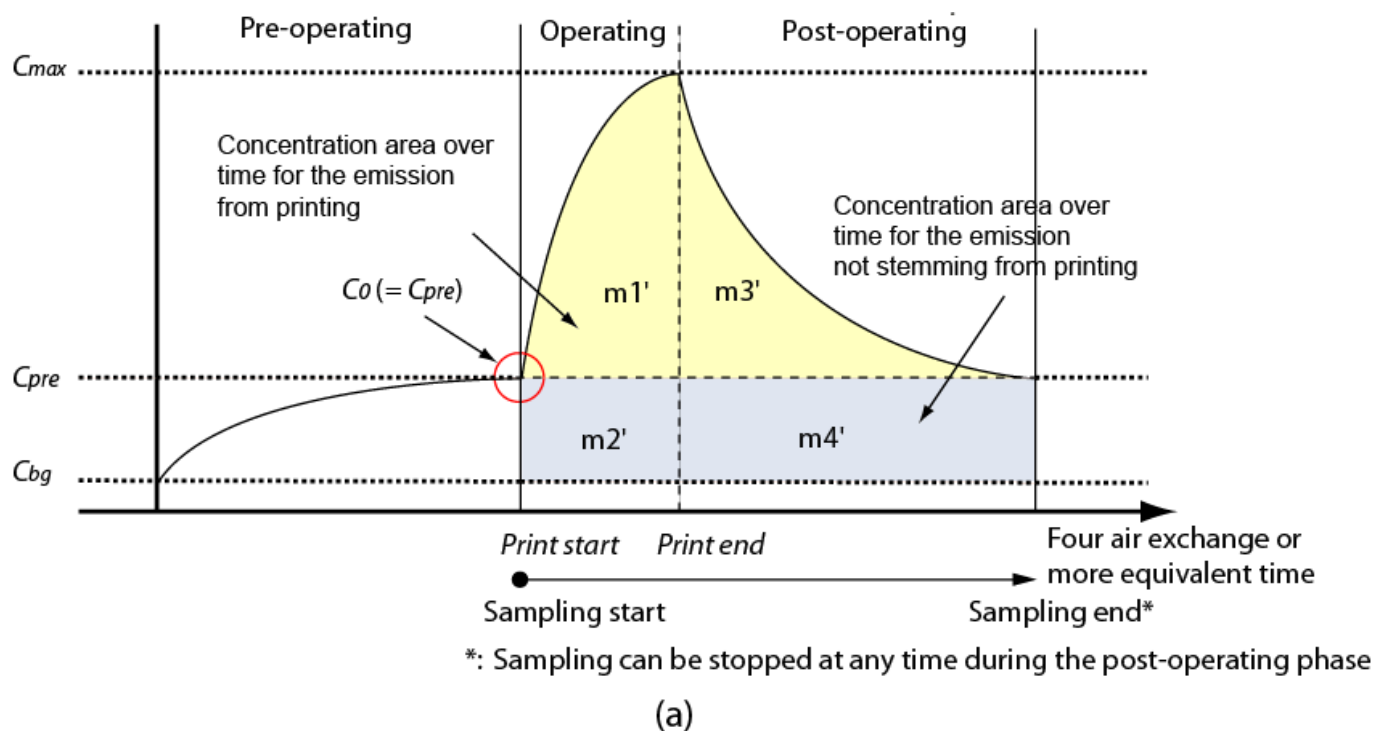


Figure C.2 — Model for equilibrium and constant  $C_o$  (a) and (b) RAL-UZ 205 Option model

The  $SER_{ope}$  is:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - (SER_{pre} + SER_{bg}) \cdot [\exp(-nt_G) + nt_G - 1] - Co \cdot n \cdot V[1 - \exp(-n \cdot t_G)]}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \quad (C.27)$$

The initial concentration ( $Co$ ) is the same as in equation (C.19) or (C.20).

If the initial concentration is equal to the pre-operating equilibrium concentration ( $Co = SER_{pre}/(n \cdot V)$ ) and  $n$  is equal in the pre-, post and operating phases (i.e. (C.19) holds), then (C.27) can be reduced to:

$$SER_{ope} = \frac{C_{ope} \cdot n^2 \cdot V \cdot t_G - SER_{pre} \cdot nt_G - SER_{bg} \cdot n \cdot t_G}{\exp(-nt_G) - \exp[-n(t_G - t_{ope})] + nt_{ope}} \quad (C.28)$$



## **Bibliography**

- [1] RAL-UZ 205, Test method for the determination of emissions from Hard Copy Devices according to RAL-UZ 205 (Appendix S-M).

